

FOXBURROW SENIORS HOUSING

Traffic Impact Study

Draft Report

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Client:

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1 INTRODUCTION

1.1 Overview

Pearlite Integrity Engineering Ltd. retained Harbourside Transportation Consultants to complete a Traffic Impact Study (TIS), as per Halifax Regional Municipality (HRM) requirements, relating to the development application for a proposed residential development on Beaver Bank Road in Beaver Bank, NS. The scope of the TIS was developed in consultation with HRM staff. The TIS follows the HRM *Guidelines for the Preparation of Traffic Impact Studies*¹.

1.2 Study Area

The subject site (PID 41517525) is located at Civic No. 328-324 Beaver Bank Road. The study area includes the segment of Beaver Bank Road between the subject site and Millwood Drive/Stokil Drive. Figure 1 illustrates the study area and the location of the subject site.

Two intersections are included in the study area:

- Beaver Bank Road and Millwood Drive/Stokil Drive (signalized), and
- Beaver Bank Road and Windgate Drive (unsignalized).

2 EXISTING TRANSPORTATION INFRASTRUCTURE

2.1 Roadways

Beaver Bank Road is a north-south arterial roadway that connects to Highway 101, Sackville Drive and the community of Beaver Bank. The posted speed limit is 60 km/h at the location of the site driveway. Along the frontage of the site, Beaver Bank Road has a two-lane cross section and a posted speed limit of 60km/h. The speed limit changes to 50 km/h approximately 90 meters south of the site driveway. There is a sidewalk on the east side of the roadway.

Millwood Drive is and east-west collector roadway that connects a residential neighbourhood to Beaver Bank Road. Millwood Drive has a two-lane cross section and a posted speed limit of 50 km/h. There is a sidewalk on the north side of the roadway near Beaver Bank Road.

Stokil Drive is an east-west collector road that a residential neighbourhood to Beaver Bank Road. Stokil Drive has a two-lane cross section and a posted speed limit of 50 km/h. There is a sidewalk on the north side of the roadway and a short segment on the south side of the roadway near Beaver Bank Road.

Windgate Drive is an east-west collector roadway that runs between Windsor Junction Road and Beaver Bank Road. Windgate Drive has a two-lane cross section and a posted speed limit is 70 km/h. There are no paved shoulders or sidewalks.

¹ Guidelines for the Preparation of Transportation Impact Studies, 8th Revision. Halifax Regional Municipality, September 2007.

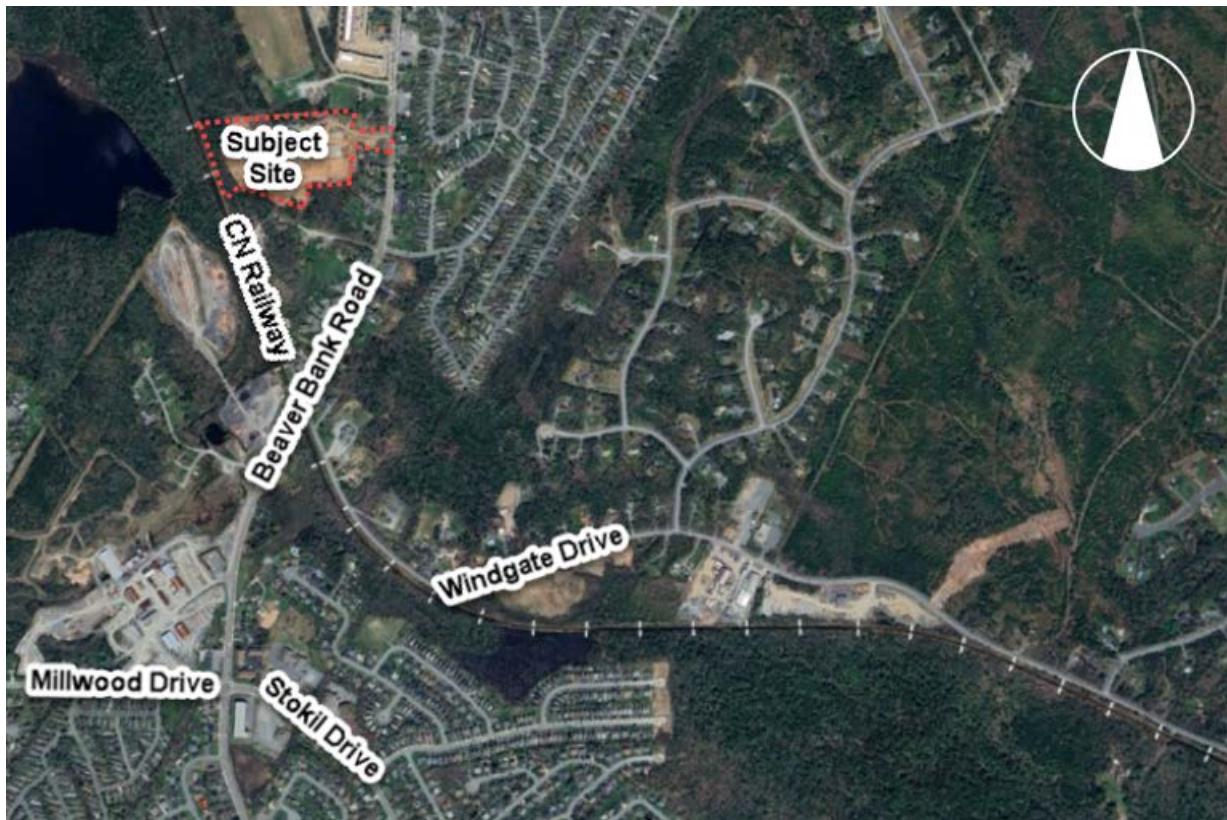


Figure 1: Site Context

2.2 Intersections

The intersection of Beaver Bank Road and Millwood Drive/Stokil Drive is a signalized intersection. All approach to the intersection include a shared through and right turn lane and an auxiliary left turn lane. There are crosswalks on all four approaches at the signalized intersection of Beaver Bank Road and Millwood Drive/Stokil Drive.

The intersection of Beaver Bank Road and Windgate Drive is an unsignalized intersection with stop-control on the Windgate Drive approach. The intersection has single lane approach except for the southbound approach which includes auxiliary left turn lane. There are rail crossing signal structures at the intersection, but the railway is not in use.

2.3 Transit

Beaver Bank Road is serviced by two Halifax Transit Route: 86 Beaver Bank and 186 Beaver Bank Express. Transit stops are located on Beaver Bank Road near the intersection with Welkin Drive, approximately 150 metres north of the site driveway.

2.4 Traffic Volumes

Recent turning movement count data at the two study intersections and a link volume count at Civic No. 345 Beaver Bank Road were obtained from HRM.

Foxburrow Senior Housing
Traffic Impact Study

Figure 2 illustrates the existing weekday morning (AM) and afternoon (PM) peak hour traffic volumes at the study intersections. **Appendix A** contains the existing count data.

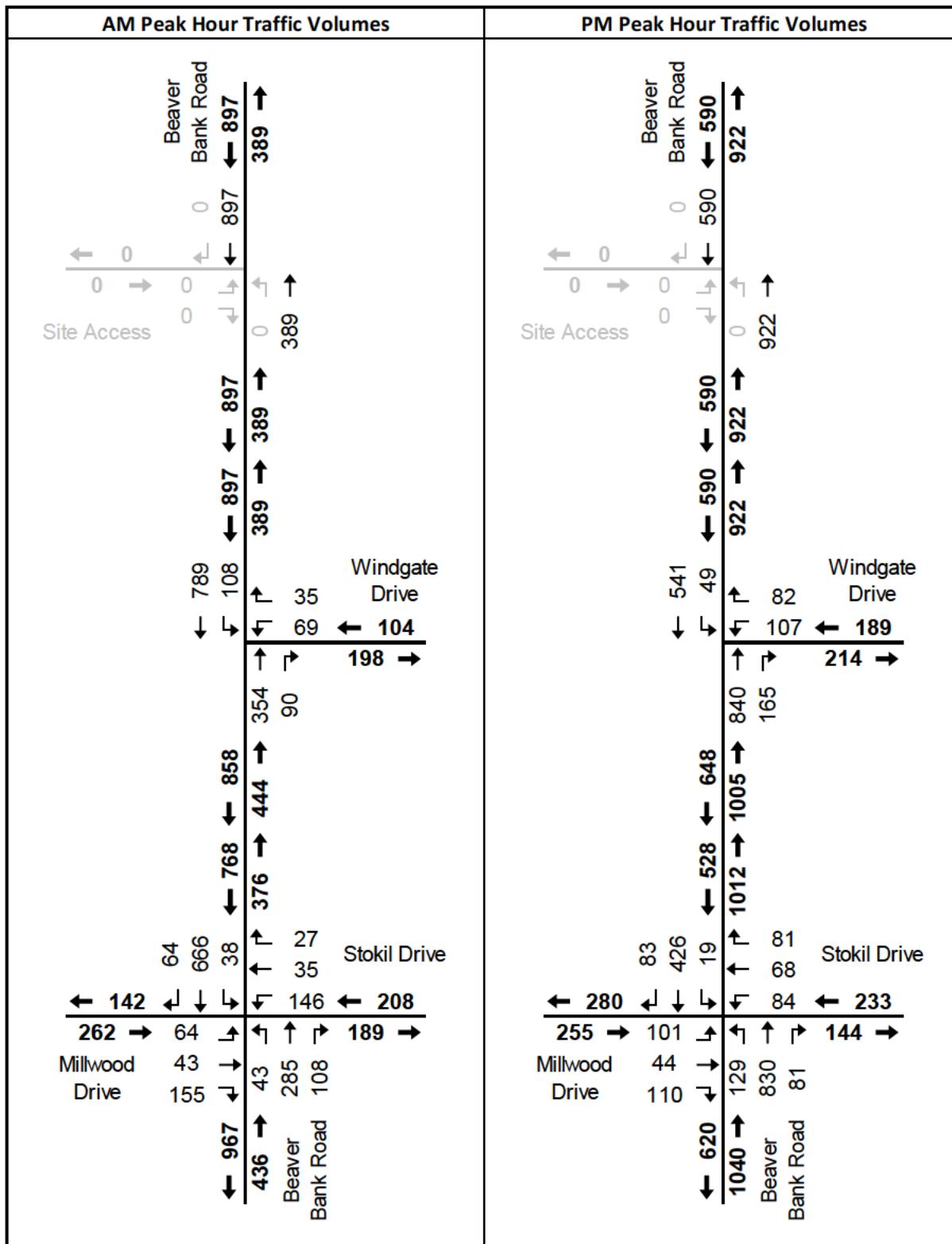


Figure 2: Existing Traffic Volumes

3 DEVELOPMENT CONCEPT

3.1 Development Description

The proposed development plan consists of three mid-rise residential buildings, with a total of 399 residential units. These units are expected to be exclusively for senior citizens. Access to the development is proposed through one driveway on Beaver Bank Road. The proposed site development plan is shown in Figure 3. The full build-out of the site is expected by 2029.

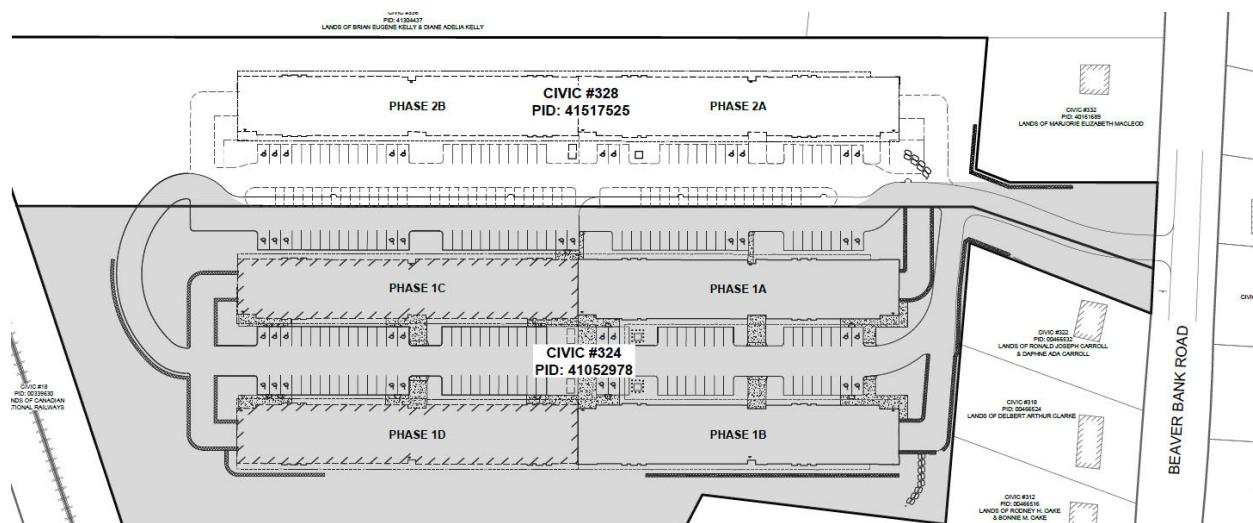


Figure 3: Site Development Plan

3.2 Access Sight Distance

A sight distance review was completed at the site access point on Beaver Bank Road to confirm that the sight lines meet the minimum stopping and intersection sight distance requirements of the Transportation Association of Canada's (TAC) *Geometric Design Guide for Canadian Roads*².

The minimum stopping and decision sight distance requirements for a two-lane roadway with a design speed of 70 km/h (posted speed limit + 10 km/h) are:

- Minimum stopping sight distance = 105 metres;
- Minimum turning sight distance – right-turn from stop = 130 metres; and
- Minimum turning sight distance – left-turn from stop = 150 metres.

The stopping sight distance requirement of 105 meters is met in both directions on Beaver Bank Road. The sight line north of the access (looking to the left) meets the minimum intersection sight distance for a right-turn of 130 meters. The sight line south of the access (looking to the right) meets the minimum intersection sight distance for a left turn of 150 meters. The sight triangles should be cleared of vegetation.

² Geometric Design Guide for Canadian Roads, Transportation Association of Canada, June 2017.

3.3 Site-Generated Traffic

3.3.1 Trip Generation

The Institute of Transportation Engineers (ITE) *Trip Generation Manual*³ was used to estimate the vehicle trip generation for the subject site. Land use code 221 Multifamily Housing (Mid-Rise), General Urban/Suburban was used for the proposed development. Table 1 summarizes the trip generation rates for the land use code.

Table 1: Trip Generation Rates

| Land Use | AM Peak Hour | | | PM Peak Hour | | |
|------------------------------------|-----------------------|----------|---------|----------------------|----------|---------|
| | Equation | Entering | Exiting | Equation | Entering | Exiting |
| 221 Multifamily Housing (Mid-Rise) | $T = 0.44(X) - 11.61$ | 23% | 77% | $T = 0.39(X) + 0.34$ | 61% | 39% |

Note: Units are in dwelling unit for residential uses.

Table 2 summarizes the weekday AM and PM peak hour trip generation estimates for the subject site . On a typical weekday, the site is estimated to generate 164 vehicle trips in the AM peak hour (38 trips entering and 126 trips exiting) and 156 vehicle trips in the PM peak hour (95 trips entering and 61 trips exiting).

Table 2: Trip Generation Estimates

| Land Use | Qty | AM Peak Hour | | | PM Peak Hour | | |
|------------------------------------|-----|--------------|----------|---------|--------------|----------|---------|
| | | Total | Entering | Exiting | Total | Entering | Exiting |
| 221 Multifamily Housing (Mid-Rise) | 399 | 164 | 38 | 126 | 156 | 95 | 61 |

Note: Units are in dwelling unit for residential uses.

3.3.2 Trip Assignment and Distribution

Site-generated trips were assigned to the site driveway on Beaver Bank Road. Trips were distributed onto Beaver Bank Road based on existing travel patterns observed in the volume count at 345 Beaver Bank Road. Table 3 summarizes the trip distribution assumptions. Trips were distributed to each turning movement at each intersection based on the existing turning movements counts.

Table 3: Trip Distribution Assumptions

| Direction of Travel | | AM | PM |
|---------------------|------------|-----|-----|
| Beaver Bank Road | Northbound | 21% | 70% |
| | Southbound | 79% | 30% |

Figure 4 illustrates the site-generated traffic volumes for the weekday AM and PM peak hours.

³ Trip Generation Manual, 11th Edition, Institute of Transportation Engineers, September 2021.

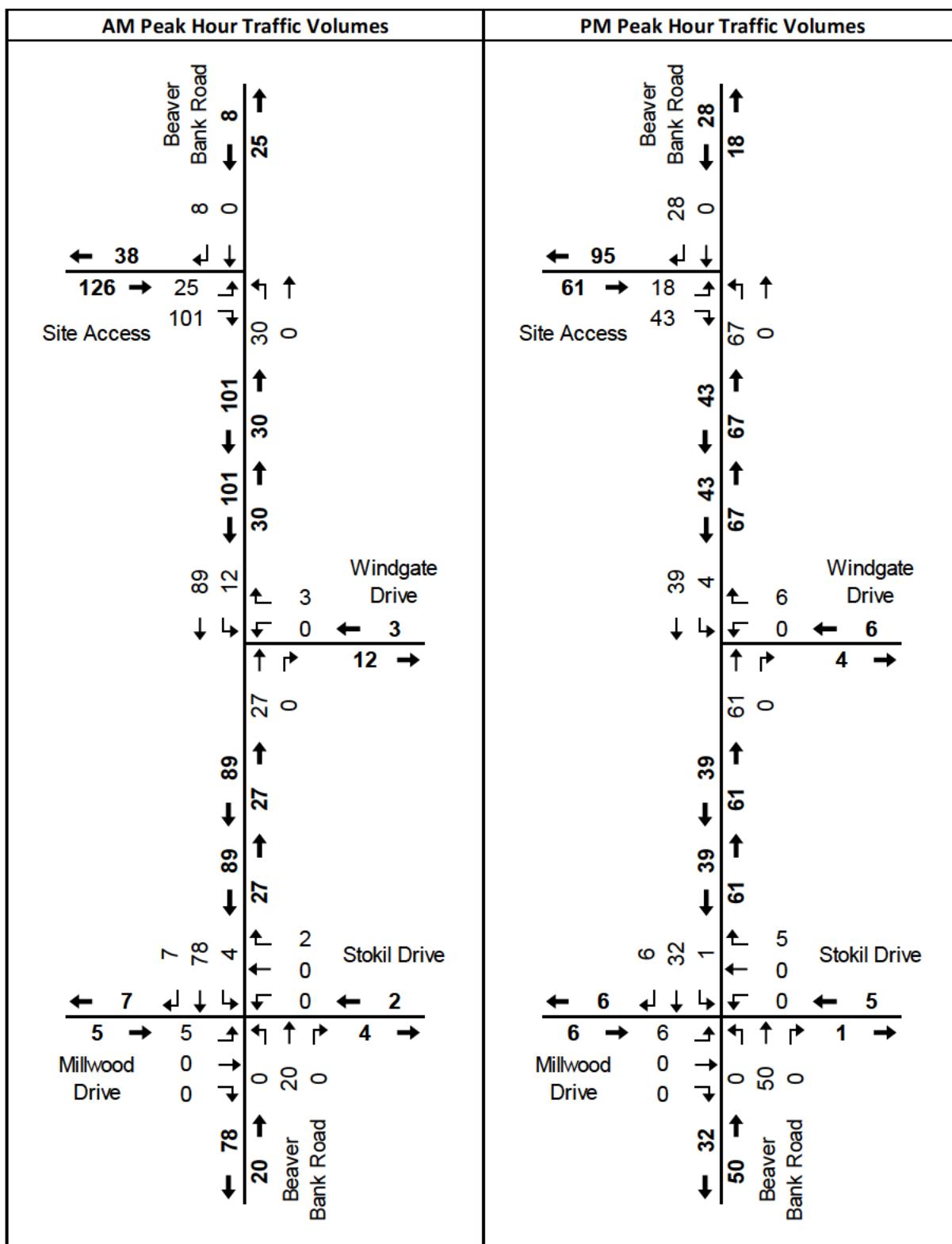


Figure 4: Site-Generated Traffic

4 TRAFFIC VOLUME FORECASTS

4.1 Study Horizon

One horizon year, five years after the full build out of the site (Year 2034) was assessed to estimate the impact of the development on the study area intersections. Future traffic volumes in the study area are estimated to consist of background traffic growth and traffic generated by the subject site.

4.2 Background Growth

Generalized background traffic growth represents growth that is expected to occur without the proposed development. The existing traffic volumes were factored using an annual growth rate of 1.0 percent to reflect background growth.

Figure 5 illustrates the future background traffic volumes for the weekday AM and PM peak hours.

4.3 Future Total Traffic Volumes

The future total traffic volumes consist of the future background volumes with the addition of the trips generated by the residential development (Refer to Figure 4).

Figure 6 illustrates the future total traffic volumes for the weekday AM and PM peak hours.

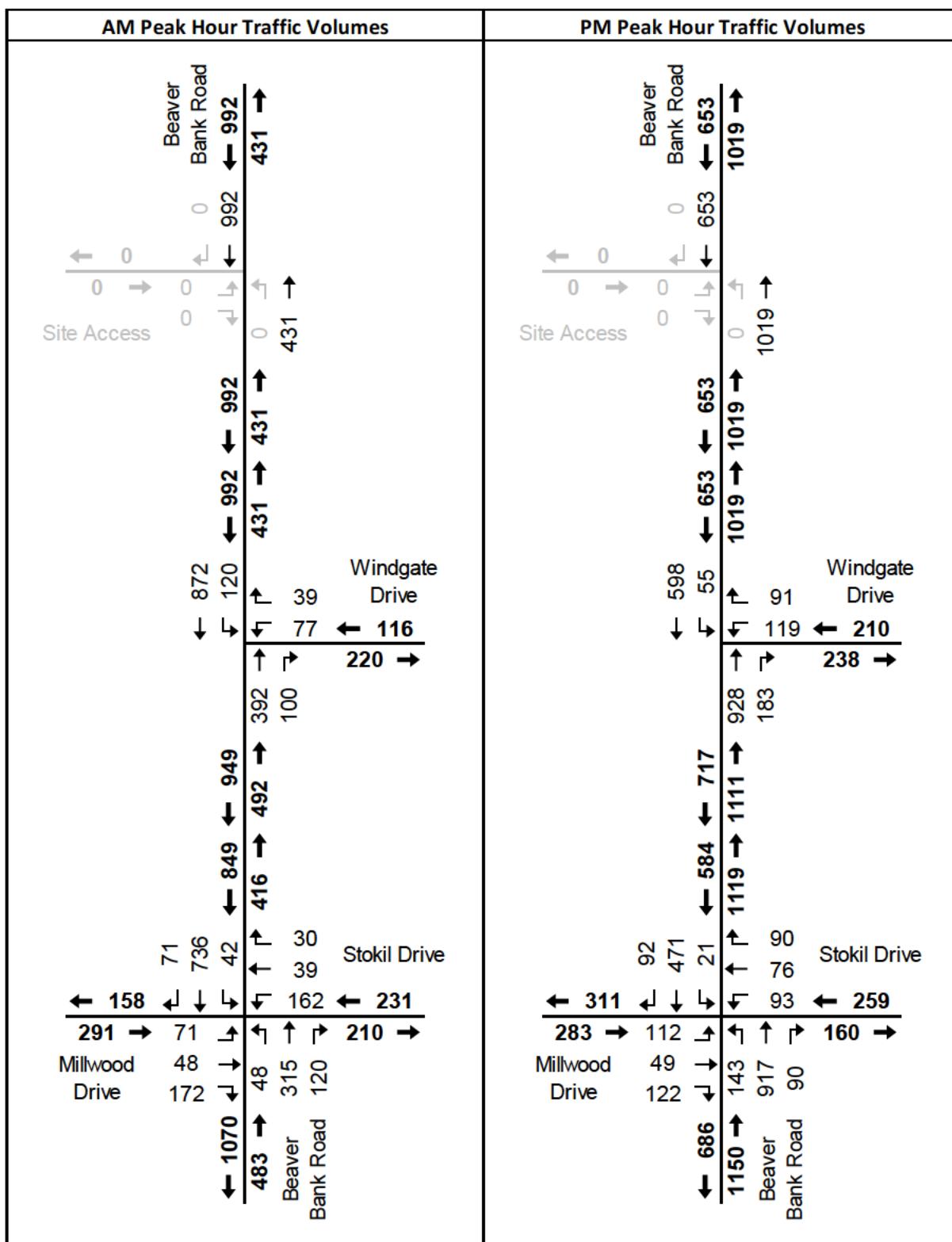


Figure 5: Future Background Traffic Volumes

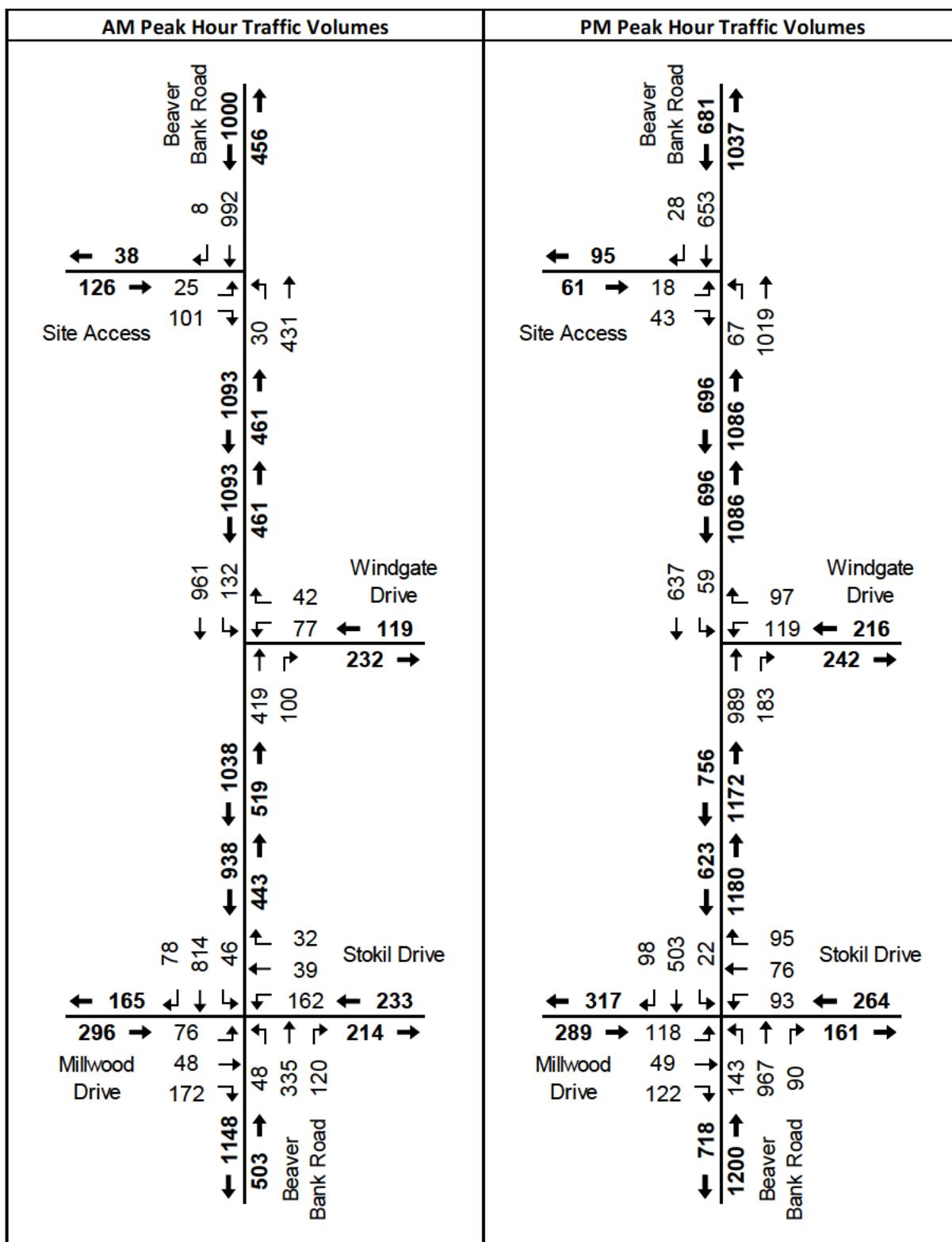


Figure 6: Future Total Traffic Volumes

5 TRAFFIC OPERATIONS ANALYSIS

5.1 Methodology

Synchro Studio 12 software was used to develop base models of the study intersections reflecting the existing weekday AM and weekday PM peak hours. Specific model input parameters include:

- Existing lane configurations and traffic control;
- Current timings and phasing for the signalized intersections (provided by HRM);
- Traffic volumes derived from the traffic counts;
- Conflicting pedestrian volumes derived from the traffic counts;
- Calculated peak hour factors (PHF) for each movement;
- Heavy vehicle percentages for each movement derived from the traffic counts; and
- Synchro default values for all other inputs.

The base models were used to assess existing operations at the study intersections. The base models were then modified to reflect future traffic volumes and the site access point to assess future operations to determine the impact of the development on traffic operations and the need for mitigation measures.

The methodology of the *Highway Capacity Manual*⁴ was used to assess the study intersections. The intersection operational analysis considered four performance measures:

- average delay per vehicle;
- level of service (LOS);
- volume-to-capacity ratio (v/c); and
- 95th percentile queue.

The criteria outlined in HRM's *Guidelines for the Preparation of Traffic Impact Studies* are used to identify critical movements:

- the overall volume-to-capacity ratio of an intersection exceeds 0.85;
- the volume-to-capacity ratio of an individual through movement or shared through/turning movement exceeds 0.85;
- the volume-to-capacity ratio of an exclusive turning movement exceeds 1.0; and
- an exclusive turning movement generates queues which exceed the available turning lane storage space.

Critical operations signify that mitigation measures may need to be considered.

5.2 Existing Operations

Traffic operations at the study intersections were evaluated using the base models. Table 4 and Table 5 summarize the results of the analysis for the AM and PM peak hours. **Appendix B** contains the supporting detailed Synchro reports.

⁴ Highway Capacity Manual, 7th edition, Transportation Research Board, 2022.

The following critical movements are identified:

- Beaver Bank Road & Millwood Drive/Stokil Drive:
 - AM: The westbound left movement (Stokil Drive) operates at LOS E. The v/c ratio for the southbound through/right movement (Beaver Bank Road) exceeds the threshold of 0.85 for a through lane (v/c = 0.87).
 - PM: The v/c ratio for the northbound through/right movement (Beaver Bank Road) exceeds the threshold of 0.85 for a through lane (v/c = 0.90).
- Beaver Bank Road & Windgate Drive:
 - AM/PM: The westbound left and right movements (Windgate Drive) operate at LOS F. The volumes for these movements exceed the capacity of the shared left/right lane (AM v/c = 1.16; PM v/c = 1.93).
 - PM: The overall intersection operates at LOS F.

Table 4: Existing Operations, AM Peak Hour

| Intersection | Control Type | Measure | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | Overall |
|---|--------------|--------------|-----------|---------|-------|----------|-----------|---------|-------|----------|------------|---------|-------|----------|------------|---------|-------|----------|---------|
| | | | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | |
| 1: Beaver Bank Road & Millwood Drive/Stokil Drive | TCS | Volume (vph) | 64 | 43 | 155 | 262 | 146 | 35 | 27 | 208 | 43 | 285 | 108 | 436 | 38 | 666 | 64 | 768 | 1674 |
| | | Delay (s) | 34.4 | 41.2 | > | 39.5 | 56.1 | 30.1 | > | 47.7 | 9.6 | 17.0 | > | 16.2 | 7.8 | 33.4 | > | 31.8 | 31.2 |
| | | LOS | C | D | > | D | E | C | > | D | A | B | > | B | A | C | > | C | C |
| | | v/c | 0.23 | 0.76 | > | | 0.74 | 0.25 | > | | 0.22 | 0.47 | > | | 0.10 | 0.87 | > | | |
| | | 95th% Q (m) | 23.5 | 42.0 | > | | 58.2 | 22.8 | > | | 8.5 | 89.5 | > | | 7.3 | 253.0 | > | | |
| | | Storage (m) | 90.0 | - | > | | 50.0 | - | > | | 90.0 | 870.0 | > | | 60.0 | 600.0 | > | | |
| 2: Beaver Bank Road & Windgate Drive | TWSC | Volume (vph) | - | - | - | | 69 | - | 35 | 104 | - | 354 | 90 | 444 | 108 | 789 | - | 897 | 1445 |
| | | Delay (s) | - | - | - | | 194.8 | - | > | ##### | - | 0 | > | 0.0 | 9.0 | 0.0 | - | 1.4 | 17.9 |
| | | LOS | - | - | - | | F | - | > | F | - | A | > | A | A | A | - | A | C |
| | | v/c | - | - | - | | 1.16 | - | > | | - | - | > | | 0.15 | - | - | | |
| | | 95th% Q (m) | - | - | - | | 8.8 | - | > | | - | 0.0 | > | | 0.5 | 0.0 | - | | |
| | | Storage (m) | - | - | - | | - | - | > | | - | 600.0 | > | | 40.0 | 340.0 | - | | |

Table 5: Existing Operations, PM Peak Hour

| Intersection | Control Type | Measure | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | Overall |
|---|--------------|--------------|-----------|---------|-------|----------|-----------|---------|-------|----------|------------|---------|-------|----------|------------|---------|-------|----------|---------|
| | | | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | |
| 1: Beaver Bank Road & Millwood Drive/Stokil Drive | TCS | Volume (vph) | 101 | 44 | 110 | 255 | 84 | 68 | 81 | 233 | 129 | 830 | 81 | 1040 | 19 | 426 | 83 | 528 | 2056 |
| | | Delay (s) | 53.7 | 32.2 | > | 42.1 | 37.2 | 52.4 | > | 47.6 | 9.6 | 34.5 | > | 30.7 | 9.1 | 21.5 | > | 20.9 | 31.9 |
| | | LOS | D | C | > | D | D | D | > | D | A | C | > | C | A | C | > | C | C |
| | | v/c | 0.71 | 0.59 | > | | 0.35 | 0.75 | > | | 0.38 | 0.90 | > | | 0.14 | 0.59 | > | | |
| | | 95th% Q (m) | 32.4 | 40.4 | > | | 29.0 | 54.9 | > | | 19.7 | 324.2 | > | | 4.2 | 132.7 | > | | |
| | | Storage (m) | 90.0 | - | > | | 50.0 | - | > | | 90.0 | 870.0 | > | | 60.0 | 600.0 | > | | |
| 2: Beaver Bank Road & Windgate Drive | TWSC | Volume (vph) | - | - | - | | 107 | - | 82 | 189 | - | 840 | 165 | 1005 | 49 | 541 | - | 590 | 1784 |
| | | Delay (s) | - | - | - | | 511.6 | - | > | ##### | - | 0 | > | 0.0 | 11.3 | 0.0 | - | 1.0 | 57.2 |
| | | LOS | - | - | - | | F | - | > | F | - | A | > | A | B | A | - | A | F |
| | | v/c | - | - | - | | 1.93 | - | > | | - | - | > | | 0.10 | - | - | | |
| | | 95th% Q (m) | - | - | - | | 18.4 | - | > | | - | 0.0 | > | | 0.3 | 0.0 | - | | |
| | | Storage (m) | - | - | - | | - | - | > | | - | 600.0 | > | | 40.0 | 340.0 | - | | |

5.3 Future Background Operations

Traffic operations at the study intersections were evaluated using the future background traffic volumes. No changes were made to the lane configuration and traffic control. Table 6 and Table 7 summarize the results of the analysis for the AM and PM peak hours. Appendix C contains the supporting detailed Synchro reports.

The following critical movements are identified:

- Beaver Bank Road & Millwood Drive/Stokil Drive:
 - AM: The westbound left movement (Stokil Drive) is expected to deteriorate to LOS F, volumes will be approaching capacity (*v/c* = 0.97). The overall westbound approach is expected to operate at LOS E. The *v/c* ratio for the southbound through/right movement (Beaver Bank Road) is expected to continue to exceed the threshold of 0.85 for a through lane (*v/c* = 0.91).
 - PM: The northbound through/right movement (Beaver Bank Road) is expected to deteriorate to LOS E, volumes are expected to exceed capacity (*v/c* = 1.01). The eastbound left movement (Millwood Drive) is expected to deteriorate to LOS E.
- Beaver Bank Road & Windgate Drive:
 - AM/PM: The westbound left and right movements (Windgate Drive) are expected to continue to operate at LOS F and exceed capacity. Operations for the overall intersection are expected to deteriorate to LOS E in the AM peak hour and continue to operate at LOS F during the PM peak hour.

Background traffic growth will contribute to the deterioration of existing operational issues at the study intersections. Mitigation measures will be required to accommodate background traffic growth at the intersection of Beaver Bank Road and Windgate Drive.

Table 6: Future Background Operations, AM Peak Hour

| Intersection | Control Type | Measure | Eastbound | | | Westbound | | | Northbound | | | Southbound | | | Overall | | | | |
|---|--------------|--------------|-----------|---------|-------|-----------|-------|---------|------------|----------|------|------------|-------|----------|---------|---------|-------|----------|------|
| | | | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | |
| 1: Beaver Bank Road & Millwood Drive/Stokil Drive | TCS | Volume (vph) | 71 | 48 | 172 | 291 | 162 | 39 | 30 | 231 | 48 | 315 | 120 | 483 | 42 | 736 | 71 | 849 | 1854 |
| | | Delay (s) | 35.4 | 49.6 | > | 46.1 | 97.4 | 31.1 | > | 76.1 | 12.1 | 17.8 | > | 17.2 | 8.3 | 38.0 | > | 36.2 | 38.1 |
| | | LOS | D | D | > | D | F | C | > | E | B | B | > | B | A | D | > | D | D |
| | | v/c | 0.27 | 0.83 | > | | 0.97 | 0.29 | > | | 0.31 | 0.49 | > | | 0.11 | 0.91 | > | | |
| | | 95th% Q (m) | 25.8 | 49.4 | > | | 63.0 | 25.3 | > | | 9.6 | 105.3 | > | | 8.2 | 308.3 | > | | |
| | | Storage (m) | 90.0 | - | > | | 50.0 | - | > | | 90.0 | 870.0 | > | | 60.0 | 600.0 | > | | |
| 2: Beaver Bank Road & Windgate Drive | TWSC | Volume (vph) | - | - | - | | 77 | - | 39 | 116 | - | 392 | 100 | 492 | 120 | 872 | - | 992 | 1600 |
| | | Delay (s) | - | - | - | | 423.9 | - | > | 424 | - | 0.0 | > | 0.0 | 9.3 | 0.0 | - | 1.4 | 38.2 |
| | | LOS | - | - | - | | F | - | > | F | - | A | > | A | A | A | - | A | E |
| | | v/c | - | - | - | | 1.69 | - | > | | - | - | > | | 0.17 | - | - | | |
| | | 95th% Q (m) | - | - | - | | 13.1 | - | > | | - | 0.0 | > | | 0.6 | 0.0 | - | | |
| | | Storage (m) | - | - | - | | - | - | > | | - | 600.0 | > | | 40.0 | 340.0 | - | | |

Table 7: Future Background Operations, PM Peak Hour

| Intersection | Control Type | Measure | Eastbound | | | Westbound | | | Northbound | | | Southbound | | | Overall | | | | |
|---|--------------|--------------|-----------|---------|-------|-----------|-------|---------|------------|----------|------|------------|-------|----------|---------|---------|-------|----------|------|
| | | | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | |
| 1: Beaver Bank Road & Millwood Drive/Stokil Drive | TCS | Volume (vph) | 112 | 49 | 122 | 283 | 93 | 76 | 90 | 259 | 143 | 917 | 90 | 1150 | 21 | 471 | 92 | 584 | 2276 |
| | | Delay (s) | 63.6 | 38.6 | > | 50.1 | 39.6 | 54.5 | > | 49.9 | 11.5 | 55.1 | > | 48.5 | 10.2 | 24.7 | > | 24.0 | 42.8 |
| | | LOS | E | D | > | D | D | > | D | B | E | > | D | B | C | > | C | D | |
| | | v/c | 0.81 | 0.69 | > | | 0.44 | 0.77 | > | | 0.46 | 1.01 | > | | 0.17 | 0.66 | > | | |
| | | 95th% Q (m) | 36.0 | 47.0 | > | | 31.8 | 62.4 | > | | 22.9 | 390.9 | > | | 4.7 | 159.2 | > | | |
| | | Storage (m) | 90.0 | - | > | | 50.0 | - | > | | 90.0 | 870.0 | > | | 60.0 | 600.0 | > | | |
| 2: Beaver Bank Road & Windgate Drive | TWSC | Volume (vph) | - | - | - | | 119 | - | 91 | 210 | - | 928 | 183 | 1111 | 55 | 598 | - | 653 | 1974 |
| | | Delay (s) | - | - | - | | 926.0 | - | > | 926 | - | 0.0 | > | 0.0 | 12.2 | 0.0 | - | 1.1 | 104 |
| | | LOS | - | - | - | | F | - | > | F | - | A | > | A | B | A | - | A | F |
| | | v/c | - | - | - | | 2.83 | - | > | | - | - | > | | 0.13 | - | - | | |
| | | 95th% Q (m) | - | - | - | | 24.3 | - | > | | - | 0.0 | > | | 0.4 | 0.0 | - | | |
| | | Storage (m) | - | - | - | | - | - | > | | - | 600.0 | > | | 40.0 | 340.0 | - | | |

5.4 Background Mitigation

5.4.1 Traffic Signal Warrant

The Transportation Association of Canada (TAC) *Traffic Signal and Pedestrian Head Warrant Handbook*⁵ provides guidance on the assessment of the need for traffic control signals at intersections. The procedure uses a “cumulative factors methodology” to identify if traffic control signals are warranted based on factors such as geometry, operating parameters, local demographics and pedestrian and vehicular volumes and conflicts. To warrant the installation of a traffic control signal, an intersection must score a minimum of 100 cumulative warrant points.

The traffic signal warrant analysis was completed for the intersection of Beaver Bank Road and Windgate Drive. **Appendix D** contains the warrant analysis worksheets. The intersection scored a total of 91 points based on existing traffic volumes and 111 points based on future background total traffic volumes. A traffic signal will be warranted at the intersection of Beaver Bank Road and Windgate Drive to accommodate background traffic volumes.

5.4.2 Future Background Operations with Mitigation

Traffic operations at the study intersections were evaluated using the future background traffic volumes and the proposed traffic signals at the intersection of Beaver Bank Road and Windgate Drive. A northbound right turn lane on Beaver Bank Road will also be required at the intersection to maintain the v/c ratio for the northbound through movement below the HRM threshold of 0.85. Signal timings were optimized at the intersection of Beaver Bank Road and Millwood Drive/Stokil Drive. Table 8 and Table 9 summarize the results of the analysis for the AM and PM peak hours. **Appendix E** contains the supporting detailed Synchro reports.

The proposed traffic signal and change to the northbound lane configuration will restore operations at the intersection of Beaver Bank Road and Windgate Drive to acceptable levels of service during both peak hours.

The following changes are identified at the intersection Beaver Bank Road and Millwood Drive/Stokil Drive with optimized signal timings:

- AM Peak Hour:
 - The westbound left movement (Stokil Drive) is expected to improve from LOS F to LOS E and the v/c ratio will improve from 0.97 to 0.83. The overall westbound approach is expected to continue to operate at LOS E, however, average delay is expected to reduce by approximately 20 seconds per vehicle.
 - The v/c ratio for the southbound through/right movement (Beaver Bank Road) is expected to increase from 0.91 to 0.93.
- PM Peak Hour:
 - The optimized timings increase the green time on Beaver Bank Road to improve operations for the over capacity northbound through movement, leading to deterioration of operations for some minor street movements.

⁶ Traffic Signal and Pedestrian Head Warrant Handbook, Transportation Association of Canada, June 2014.

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- The northbound through/right movement (Beaver Bank Road) is expected to improve from LOS E to LOS D and the v/c ratio will improve from 1.01 to 0.95. Average delay on the northbound approach is expected to reduce by approximately 12 seconds per vehicle.
- The eastbound left movement (Millwood Drive) is expected to deteriorate from LOS E to LOS F and the v/c ratio will deteriorate from 0.81 to 0.97.
- The westbound through/right movement (Stokil Drive) is expected to deteriorate to LOS E, the v/c ratio for the movement will remain below the threshold of 0.85.

Changes to the signal timings cannot restore operations to acceptable levels of service at the intersection Beaver Bank Road and Millwood Drive/Stokil Drive. Increasing capacity at the intersection would require widening Beaver Bank Road. It is noted that there are long term plans for the extension of Margeson Drive north of Trunk 1, this parallel route may provide some traffic relief to Beaver Bank Road.

Table 8: Future Background Operations with Mitigation, AM Peak Hour

| Intersection | Control Type | Measure | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | Overall |
|---|--------------|--------------|-----------|---------|-------|----------|-----------|---------|-------|----------|------------|---------|-------|----------|------------|---------|-------|----------|---------|
| | | | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | |
| 1: Beaver Bank Road & Millwood Drive/Stokil Drive | TCS | Volume (vph) | 71 | 48 | 172 | 291 | 162 | 39 | 30 | 231 | 48 | 315 | 120 | 483 | 42 | 763 | 71 | 876 | 1881 |
| | | Delay (s) | 38.2 | 53.5 | > | 49.7 | 66.9 | 32.0 | > | 55.7 | 13.2 | 18.1 | > | 17.6 | 8.4 | 41.8 | > | 39.7 | 37.9 |
| | | LOS | D | D | > | D | E | C | > | E | B | B | > | B | A | D | > | D | D |
| | | v/c | 0.28 | 0.84 | > | | 0.83 | 0.25 | > | | 0.33 | 0.50 | > | | 0.12 | 0.93 | > | | |
| | | 95th% Q (m) | 27.1 | 53.7 | > | | 65.6 | 26.2 | > | | 9.1 | 99.4 | > | | 7.7 | 296.8 | > | | |
| | | Storage (m) | 90.0 | - | > | | 50.0 | - | > | | 90.0 | 870.0 | > | | 60.0 | 600.0 | > | | |
| 2: Beaver Bank Road & Windgate Drive | TCS | Volume (vph) | - | - | - | | 77 | - | 39 | 116 | - | 392 | 100 | 492 | 120 | 872 | - | 992 | 1600 |
| | | Delay (s) | - | - | - | | 29.9 | - | > | 29.9 | - | 7 | 1.5 | 5.8 | 7.4 | 16.3 | - | 14.9 | 13.5 |
| | | LOS | - | - | - | | C | - | > | C | - | A | A | A | A | B | - | B | B |
| | | v/c | - | - | - | | 0.52 | - | > | | - | 0.36 | 0.12 | | 0.29 | 0.8 | - | | |
| | | 95th% Q (m) | - | - | - | | 27.0 | - | > | | - | 48.3 | 4.1 | | 15.8 | 175.8 | - | | |
| | | Storage (m) | - | - | - | | - | - | > | | - | 600.0 | 25.0 | | 40.0 | 340.0 | - | | |

Table 9: Future Background Operations with Mitigation, PM Peak Hour

| Intersection | Control Type | Measure | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | Overall |
|---|--------------|--------------|-----------|---------|-------|----------|-----------|---------|-------|----------|------------|---------|-------|----------|------------|---------|-------|----------|---------|
| | | | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | |
| 1: Beaver Bank Road & Millwood Drive/Stokil Drive | TCS | Volume (vph) | 112 | 49 | 122 | 283 | 93 | 76 | 90 | 259 | 143 | 917 | 90 | 1150 | 21 | 471 | 92 | 584 | 2276 |
| | | Delay (s) | 104.1 | 45.0 | > | 72.2 | 49.2 | 62.3 | > | 58.2 | 9.9 | 41.4 | > | 36.6 | 9.7 | 21.9 | > | 21.3 | 40.6 |
| | | LOS | F | D | > | E | D | E | > | E | A | D | > | D | A | C | > | C | D |
| | | v/c | 0.97 | 0.73 | > | | 0.53 | 0.81 | > | | 0.43 | 0.95 | > | | 0.19 | 0.62 | > | | |
| | | 95th% Q (m) | 39.2 | 50.8 | > | | 34.4 | 66.6 | > | | 20.8 | 381.9 | > | | 4.3 | 150.9 | > | | |
| | | Storage (m) | 90.0 | - | > | | 50.0 | - | > | | 90.0 | 870.0 | > | | 60.0 | 600.0 | > | | |
| 2: Beaver Bank Road & Windgate Drive | TCS | Volume (vph) | - | - | - | | 119 | - | 91 | 210 | - | 928 | 183 | 1111 | 55 | 598 | - | 653 | 1974 |
| | | Delay (s) | - | - | - | | 37.8 | - | > | 37.8 | - | 18.9 | 3.7 | 16.2 | 18.5 | 11.0 | - | 11.7 | 17.0 |
| | | LOS | - | - | - | | D | - | > | D | - | B | A | B | B | B | - | B | B |
| | | v/c | - | - | - | | 0.69 | - | > | | - | 0.84 | 0.21 | | 0.45 | 0.6 | - | | |
| | | 95th% Q (m) | - | - | - | | 58.7 | - | > | | - | 183.1 | 13.6 | | 13.1 | 82.8 | - | | |
| | | Storage (m) | - | - | - | | - | - | > | | - | 600.0 | 25.0 | | 40.0 | 340.0 | - | | |

5.5 Future Total Operations

Traffic operations at the study intersections and the proposed site driveway were evaluated using the future total traffic volumes. The proposed mitigation measures required to accommodate background growth are included in this scenario. The proposed site access intersection was modelled with a northbound left turn lane on Beaver Bank Road and a shared left/right lane on the driveway approach. Refer to Section 6 for the left turn lane warrant analysis.

Table 10 and Table 11 summarizes the results of the analysis for the AM and PM peak hours. **Appendix F** contains the supporting detailed Synchro reports.

The following critical movements are identified:

- Beaver Bank Road & Millwood Drive/Stokil Drive:
 - AM: The eastbound through/right movement (Millwood Drive) is expected to deteriorate to LOS E and the v/c ratio is expected to exceed the threshold of 0.85 for a through lane ($v/c = 0.87$). The westbound left movement (Stokil Drive) is expected to continue to operate at LOS E. The v/c ratio for the southbound through (Beaver Bank Road) is expected to increase from 0.93 to 0.98. Average delay per vehicle at the intersection is expected to increase by approximately 5.5 seconds per vehicle.
 - PM: The eastbound left movement (Millwood Drive) is expected to continue to operate at LOS F and is expected to exceed capacity. The overall eastbound approach will deteriorate from LOS E to LOS F. The westbound through movement (Stokil Drive) is expected to continue to operate at LOS E. The v/c ratio for the northbound through is expected to increase from 0.95 to 1.00. Average delay per vehicle at the intersection is expected to increase by approximately 6.0 seconds per vehicle.
- Beaver Bank Road & Site Access:
 - AM: The eastbound left and right movements (Site Access) are expected to operate at LOS F, however, the v/c ratio is expected to be well below the threshold of 0.85 for a shared lane ($v/c = 0.67$).
 - PM: The eastbound left and right movements (Site Access) are expected to operate at LOS E, however, the v/c ratio is expected to be well below the threshold of 0.85 for a shared lane ($v/c = 0.42$).

There are existing and background operational issues at the intersection of Beaver Bank Road and Millwood Drive/Stokil Drive. As previously noted, these issues cannot be significantly improved without the widening of Beaver Bank Road or the provision of an alternative route. As a result, these issues will continue to deteriorate with the addition of the site generated traffic. Volumes on Beaver Bank Road are expected to be near or over the capacity of a single through lane. It is noted that traffic generated by the development is expected to account for approximately 6% of total traffic volume at the intersection during the AM peak hour and approximately 4% during the PM peak hour.

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Table 10: Future Total Operations, AM Peak Hour

| Intersection | Control Type | Measure | Eastbound | | | Westbound | | | Northbound | | | Southbound | | | Overall | | | | |
|---|--------------|--------------|-----------|---------|-------|-----------|------|---------|------------|----------|-------|------------|-------|----------|---------|-------|------|------|------|
| | | | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | | | | | |
| 1: Beaver Bank Road & Millwood Drive/Stokil Drive | TCS | Volume (vph) | 76 | 48 | 172 | 296 | 162 | 39 | 32 | 233 | 48 | 335 | 120 | 503 | 46 | 814 | 78 | 938 | 1970 |
| | | Delay (s) | 39.5 | 57.6 | > | 52.9 | 76.4 | 31.9 | > | 61.8 | 16.3 | 18.0 | > | 17.8 | 8.4 | 51.0 | > | 48.4 | 43.3 |
| | | LOS | D | E | > | D | E | C | > | E | B | B | > | B | A | D | > | D | D |
| | | v/c | 0.32 | 0.87 | > | | 0.88 | 0.31 | > | | 0.36 | 0.50 | > | | 0.13 | 0.98 | > | | |
| | | 95th% Q (m) | 28.6 | 53.7 | > | | 62.0 | 26.5 | > | | 9.8 | 106.1 | > | | 8.4 | 350.6 | > | | |
| | | Storage (m) | 90.0 | - | > | | 50.0 | - | > | | 90.0 | 870.0 | > | | 60.0 | 600.0 | > | | |
| 2: Beaver Bank Road & Windgate Drive | TCS | Volume (vph) | - | - | - | 77 | - | 42 | 119 | - | 419 | 100 | 519 | 132 | 961 | - | 1093 | 1731 | |
| | | Delay (s) | - | - | - | | 36.6 | - | > | 36.6 | - | 6.6 | 1.3 | 5.5 | 7.2 | 17.9 | - | 16.3 | 14.9 |
| | | LOS | - | - | - | D | - | > | D | - | A | A | A | A | B | - | B | B | |
| | | v/c | - | - | - | 0.57 | - | > | | - | 0.36 | 0.11 | | 0.31 | 0.84 | - | | | |
| | | 95th% Q (m) | - | - | - | 31.5 | - | > | | - | 51.0 | 3.8 | | 17.1 | 216.6 | - | | | |
| | | Storage (m) | - | - | - | - | - | > | | - | 600.0 | 25.0 | | 40.0 | 340.0 | - | | | |
| 3: Beaver Bank Road & Site Access | TWSC | Volume (vph) | 25 | - | 101 | 126 | - | - | - | | 30 | 431 | - | 461 | - | 992 | 8 | 1000 | 1587 |
| | | Delay (s) | 51.8 | - | > | 51.8 | - | - | - | | 10.9 | 0.0 | - | 0.7 | - | 0.0 | > | 0.0 | 4.3 |
| | | LOS | F | - | > | F | - | - | - | | B | A | - | A | - | A | > | A | A |
| | | v/c | 0.67 | - | > | | - | - | - | | 0.05 | - | - | - | - | - | > | | |
| | | 95th% Q (m) | 4.1 | - | > | | - | - | - | | 0.2 | 0.0 | - | - | - | 0.0 | > | | |
| | | Storage (m) | 0.0 | - | > | | - | - | - | | 25.0 | - | - | - | - | - | > | | |

Table 11: Future Total Operations, PM Peak Hour

| Intersection | Control Type | Measure | Eastbound | | | Westbound | | | Northbound | | | Southbound | | | Overall | | | | |
|---|--------------|--------------|-----------|---------|-------|-----------|------|---------|------------|----------|-------|------------|-------|----------|---------|---------|-------|----------|------|
| | | | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | Left | Through | Right | Approach | |
| 1: Beaver Bank Road & Millwood Drive/Stokil Drive | TCS | Volume (vph) | 118 | 49 | 122 | 289 | 93 | 76 | 95 | 264 | 143 | 967 | 90 | 1200 | 22 | 503 | 98 | 623 | 2376 |
| | | Delay (s) | 121.0 | 44.2 | > | 80.4 | 48.7 | 63.0 | > | 58.6 | 10.7 | 52.2 | > | 46.1 | 10.0 | 23.6 | > | 23.0 | 46.6 |
| | | LOS | F | D | > | F | D | E | > | E | B | D | > | D | A | C | > | C | D |
| | | v/c | 1.04 | 0.72 | > | | 0.52 | 0.82 | > | | 0.46 | 1.00 | > | | 0.19 | 0.66 | > | | |
| | | 95th% Q (m) | 41.9 | 50.8 | > | | 34.4 | 68.6 | > | | 20.7 | 410.8 | > | | 4.4 | 168.9 | > | | |
| | | Storage (m) | 90.0 | - | > | | 50.0 | - | > | | 90.0 | 870.0 | > | | 60.0 | 600.0 | > | | |
| 2: Beaver Bank Road & Windgate Drive | TCS | Volume (vph) | - | - | - | 119 | - | 97 | 216 | - | 989 | 183 | 1172 | 59 | 637 | - | 696 | 2084 | |
| | | Delay (s) | - | - | - | 44.4 | - | > | 44.4 | - | 20.5 | 3.8 | 17.7 | 27.4 | 11.3 | - | 12.7 | 18.8 | |
| | | LOS | - | - | - | D | - | > | D | - | C | A | B | C | B | - | B | B | |
| | | v/c | - | - | - | 0.73 | - | > | | - | 0.86 | 0.20 | | 0.56 | 0.63 | - | | | |
| | | 95th% Q (m) | - | - | - | 67.1 | - | > | | - | 215.4 | 14.3 | | 17.9 | 92.7 | - | | | |
| | | Storage (m) | - | - | - | - | - | > | | - | 600.0 | 25.0 | | 40.0 | 340.0 | - | | | |
| 3: Beaver Bank Road & Site Access | TWSC | Volume (vph) | 18 | - | 43 | 61 | - | - | - | | 67 | 1019 | - | 1086 | - | 653 | 28 | 681 | 1828 |
| | | Delay (s) | 44.1 | - | > | 44.1 | - | - | - | | 9.5 | 0.0 | - | 0.6 | - | 0.0 | > | 0.0 | 1.8 |
| | | LOS | E | - | > | E | - | - | - | | A | A | - | A | - | A | > | A | A |
| | | v/c | 0.42 | - | > | | - | - | - | | 0.08 | - | - | - | - | - | > | | |
| | | 95th% Q (m) | 1.9 | - | > | | - | - | - | | 0.3 | 0.0 | - | - | - | 0.0 | > | | |
| | | Storage (m) | 0.0 | - | > | | - | - | - | | 25.0 | - | - | - | - | - | > | | |

6 LEFT TURN LANE WARRANT

The Ministry of Transportation of Ontario (MTO) *Design Supplement for the TAC Geometric Design Guide for Canadian Roads*⁶ provides guidance on the assessment of the need for left turn lanes at unsignalized intersections. The methodology uses a series of nomographs to identify if a left turn lane is warranted based on factors such as design speed, advancing volumes, and left turn volume as a percentage of advancing volumes and opposing volumes.

The left turn lane warrant analysis was completed for the northbound left turn from Beaver Bank Road onto the proposed site driveway using the future total traffic volumes. A design speed of 70 km/h (posted speed limit + 10 km/h) was used for the left turn lane warrant analysis.

Figure 7 illustrates the left turn warrant analysis. The northbound left turn volume is expected to represent approximately 6% of the advancing volume during both peak hours. The analysis indicates that a northbound left turn lane with a storage length of 25 metres will be warranted on Beaver Bank Road at the site driveway.

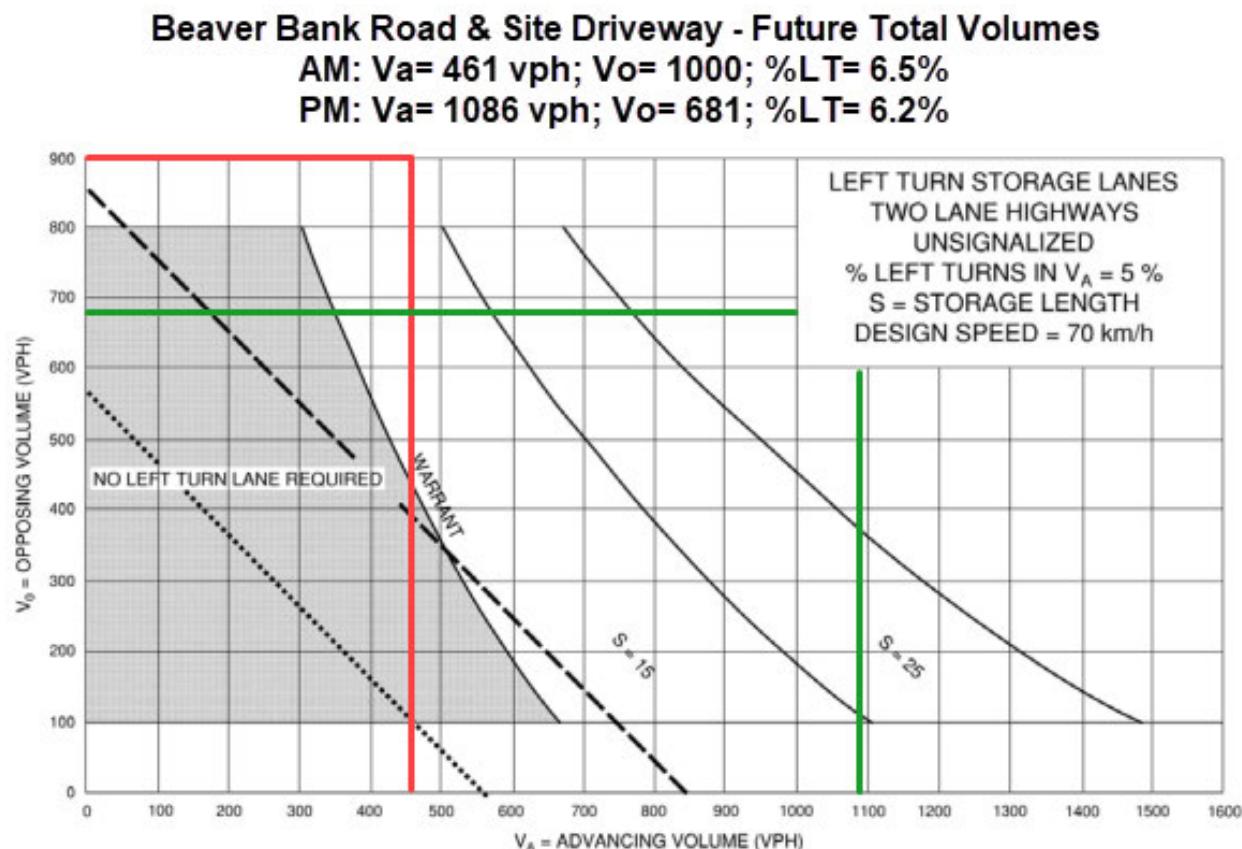


Figure 7: Left Turn Lane Warrant for Site Driveway

⁵ Design Supplement for TAC Geometric Design Guide for Canadian Roads, Appendix 9 for Chapter 9 Intersections, Ministry of Transportation of Ontario, June 2017.

7 CONCLUSIONS AND RECOMMENDATIONS

7.1 Conclusions

Pearlite Integrity Engineering Ltd. retained Harbourside Transportation Consultants to complete a Traffic Impact Study, as per Halifax Regional Municipality (HRM) requirements, for a residential development at Civic No. 328-324 Beaver Bank Road in Beaver Bank, NS.

The proposed residential development will consist of three buildings, with a total of 399 residential units. The units are expected to be exclusively for senior citizens. Access to the site is proposed through a driveway on Beaver Bank Road.

Based on the investigations carried out, it is concluded that:

- **Site-Generated Traffic:** The residential development is estimated to generate 164 trips in the AM peak hour and 156 trips in the PM peak hour.
- **Access Sight Distance:** The site access is expected to have adequate intersection and stopping sight distances.
- **Existing Operations:** There are existing operational concerns at the intersection of Beaver Bank Road and Millwood Drive/Stokil Drive for the through movements on Beaver Bank Road. There are also existing operational concerns at the intersection of Beaver Bank Road and Windgate Drive for the Windgate Drive approach.
- **Future Background Operations:** Background traffic growth will contribute to the deterioration of existing operational issues at the study intersections. Mitigation measures will be required to accommodate background traffic growth at the intersection of Beaver Bank Road and Windgate Drive. Traffic signals will be warranted at the intersection of Beaver Bank Road and Windgate Drive.
- **Future Background Operations with Mitigations:** Traffic signals and the addition of a northbound right turn lane is expected to restore operations to acceptable levels of service at the intersection of Beaver Bank Road and Windgate Drive. Changes to the signal timings can improve operations at the intersection of Beaver Bank Road and Millwood Drive/Stokil Drive, however, operational issues will remain without significant improvements to increase capacity such as widening Beaver Bank Road or providing an alternative corridor.
- **Future Total Operations:** The existing and background operational issues at the intersection of Beaver Bank Road and Millwood Drive/Stokil Drive will continue to deteriorate with the addition of the site generated traffic. Volumes on Beaver Bank Road are expected to be near or over the capacity of a single through lane. Traffic generated by the development is expected to account for approximately 6% of total traffic volume at the intersection during the AM peak hour and approximately 4% during the PM peak hour. The intersection of Beaver Bank Road and Windgate Drive will operate at adequate levels of service.
- **Left Turn Lane Warrant:** A left turn lane with 25 meters of storage will be warranted for the northbound left turn at the site driveway on Beaver Bank Road.

7.2 Recommendations

Based on the findings of the study, the following mitigation measures are recommended:

- Signal timings should be adjusted at the intersection of Beaver Bank Road and Millwood Drive/Stokil Drive as development progresses.
- A left turn lane should be provided on Beaver Bank Road at the proposed site driveway. The left turn lane should provide a minimum of 25 meters of storage length.
- Traffic signals and a northbound right turn lane should be implemented at the intersection of Beaver Bank Road and Windgate Drive. It is noted that this improvement is required to accommodate background traffic growth and is required without the proposed development.

APPENDIX A: TRAFFIC COUNT DATA

Turning Movement Data

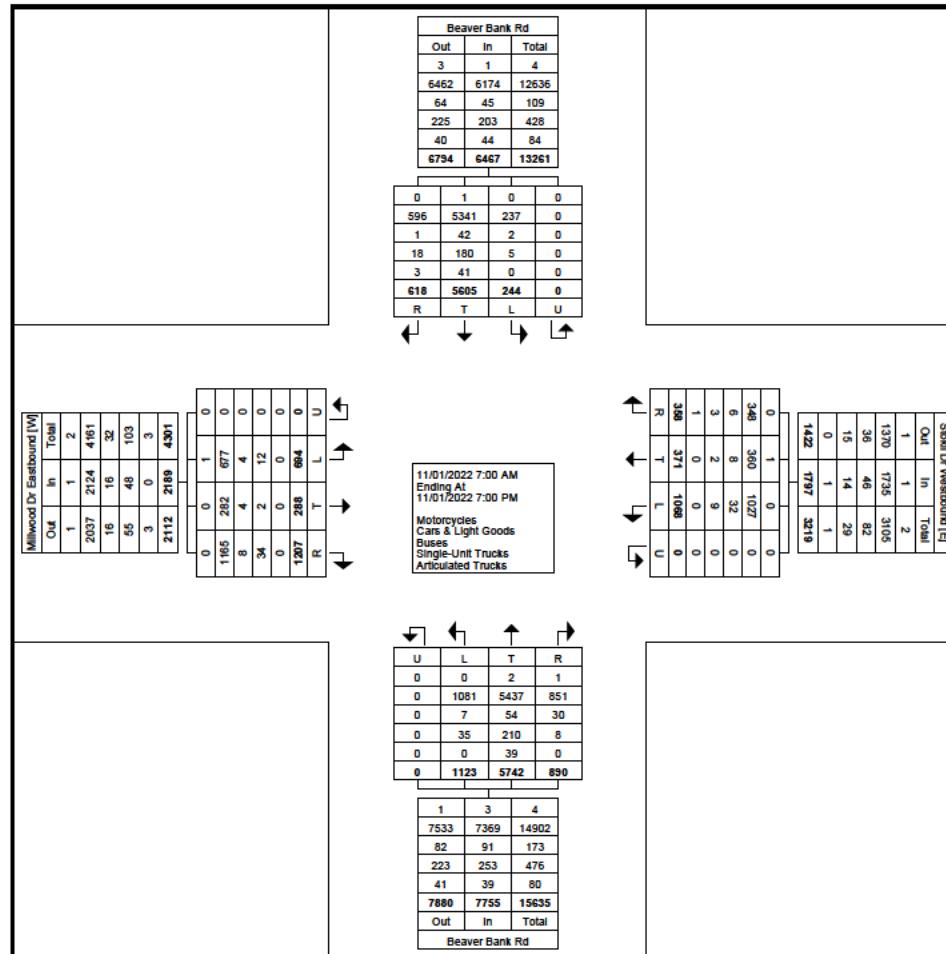
| Start Time | Beaver Bank Rd Southbound | | | | | Stokil Dr Westbound | | | | | Beaver Bank Rd Northbound | | | | | Millwood Dr Eastbound | | | | | Int. Total | |
|--------------|---------------------------|------|------|--------|------------|---------------------|------|------|--------|------------|---------------------------|------|------|--------|------------|-----------------------|------|------|--------|------------|------------|--|
| | Southbound | | | | | Westbound | | | | | Northbound | | | | | Eastbound | | | | | | |
| | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | | |
| 7:00 AM | 17 | 223 | 5 | 0 | 245 | 6 | 10 | 31 | 0 | 47 | 9 | 43 | 7 | 0 | 59 | 30 | 4 | 13 | 0 | 47 | 398 | |
| 7:15 AM | 13 | 198 | 6 | 0 | 217 | 7 | 9 | 27 | 0 | 43 | 12 | 58 | 4 | 0 | 74 | 31 | 7 | 9 | 0 | 47 | 381 | |
| 7:30 AM | 15 | 192 | 5 | 0 | 212 | 10 | 9 | 34 | 0 | 53 | 26 | 73 | 8 | 0 | 107 | 36 | 6 | 17 | 0 | 59 | 431 | |
| 7:45 AM | 16 | 164 | 10 | 0 | 190 | 5 | 8 | 33 | 0 | 46 | 29 | 64 | 13 | 0 | 106 | 38 | 10 | 13 | 0 | 61 | 403 | |
| Hourly Total | 61 | 777 | 26 | 0 | 864 | 28 | 36 | 125 | 0 | 189 | 76 | 238 | 32 | 0 | 346 | 135 | 27 | 52 | 0 | 214 | 1613 | |
| 8:00 AM | 24 | 171 | 14 | 0 | 209 | 7 | 10 | 42 | 0 | 59 | 25 | 69 | 10 | 0 | 104 | 46 | 14 | 20 | 0 | 80 | 452 | |
| 8:15 AM | 9 | 139 | 9 | 0 | 157 | 5 | 8 | 37 | 0 | 50 | 28 | 79 | 12 | 0 | 119 | 35 | 13 | 14 | 0 | 62 | 388 | |
| 8:30 AM | 11 | 183 | 5 | 0 | 199 | 3 | 9 | 33 | 0 | 45 | 19 | 65 | 25 | 0 | 109 | 30 | 7 | 10 | 0 | 47 | 400 | |
| 8:45 AM | 11 | 155 | 5 | 0 | 171 | 4 | 8 | 26 | 0 | 38 | 11 | 67 | 21 | 0 | 99 | 38 | 5 | 10 | 0 | 53 | 361 | |
| Hourly Total | 55 | 648 | 33 | 0 | 736 | 19 | 35 | 138 | 0 | 192 | 83 | 280 | 68 | 0 | 431 | 149 | 39 | 54 | 0 | 242 | 1601 | |
| 9:00 AM | 15 | 97 | 3 | 0 | 115 | 4 | 0 | 22 | 0 | 26 | 8 | 69 | 24 | 0 | 101 | 43 | 4 | 7 | 0 | 54 | 296 | |
| 9:15 AM | 12 | 130 | 8 | 0 | 150 | 2 | 6 | 22 | 0 | 30 | 11 | 71 | 14 | 0 | 96 | 22 | 1 | 11 | 0 | 34 | 310 | |
| 9:30 AM | 6 | 128 | 2 | 0 | 136 | 0 | 4 | 23 | 0 | 27 | 16 | 87 | 15 | 0 | 118 | 24 | 1 | 12 | 0 | 37 | 318 | |
| 9:45 AM | 9 | 121 | 3 | 0 | 133 | 4 | 4 | 24 | 0 | 32 | 8 | 83 | 14 | 0 | 105 | 14 | 3 | 7 | 0 | 24 | 294 | |
| Hourly Total | 42 | 476 | 16 | 0 | 534 | 10 | 14 | 91 | 0 | 115 | 43 | 310 | 67 | 0 | 420 | 103 | 9 | 37 | 0 | 149 | 1218 | |
| 10:00 AM | 6 | 105 | 2 | 0 | 113 | 2 | 5 | 19 | 0 | 26 | 9 | 82 | 12 | 0 | 103 | 21 | 4 | 3 | 0 | 28 | 270 | |
| 10:15 AM | 8 | 106 | 1 | 0 | 115 | 7 | 7 | 16 | 0 | 30 | 4 | 87 | 11 | 0 | 102 | 18 | 6 | 12 | 0 | 36 | 283 | |
| 10:30 AM | 8 | 94 | 7 | 0 | 109 | 4 | 6 | 17 | 0 | 27 | 6 | 90 | 9 | 0 | 105 | 14 | 3 | 13 | 0 | 30 | 271 | |
| 10:45 AM | 16 | 104 | 6 | 0 | 126 | 3 | 3 | 21 | 0 | 27 | 14 | 86 | 15 | 0 | 115 | 11 | 4 | 6 | 0 | 21 | 289 | |
| Hourly Total | 38 | 409 | 16 | 0 | 463 | 16 | 21 | 73 | 0 | 110 | 33 | 345 | 47 | 0 | 425 | 64 | 17 | 34 | 0 | 115 | 1113 | |
| 11:00 AM | 10 | 108 | 2 | 0 | 120 | 6 | 3 | 19 | 0 | 28 | 16 | 99 | 17 | 0 | 132 | 25 | 4 | 10 | 0 | 39 | 319 | |
| 11:15 AM | 8 | 82 | 3 | 0 | 93 | 2 | 4 | 19 | 0 | 25 | 15 | 96 | 17 | 0 | 128 | 29 | 0 | 15 | 0 | 44 | 290 | |
| 11:30 AM | 8 | 104 | 5 | 0 | 117 | 4 | 2 | 16 | 0 | 22 | 17 | 98 | 24 | 0 | 139 | 15 | 0 | 10 | 0 | 25 | 303 | |
| 11:45 AM | 9 | 129 | 0 | 0 | 138 | 2 | 6 | 24 | 0 | 32 | 23 | 99 | 35 | 0 | 157 | 18 | 8 | 16 | 0 | 42 | 369 | |
| Hourly Total | 35 | 423 | 10 | 0 | 468 | 14 | 15 | 78 | 0 | 107 | 71 | 392 | 93 | 0 | 556 | 87 | 12 | 51 | 0 | 150 | 1281 | |
| 12:00 PM | 9 | 122 | 5 | 0 | 136 | 3 | 7 | 20 | 0 | 30 | 19 | 98 | 21 | 0 | 138 | 22 | 4 | 14 | 0 | 40 | 344 | |
| 12:15 PM | 11 | 89 | 5 | 0 | 105 | 5 | 3 | 15 | 0 | 23 | 17 | 104 | 17 | 0 | 138 | 21 | 4 | 7 | 0 | 32 | 298 | |
| 12:30 PM | 4 | 119 | 3 | 0 | 126 | 3 | 9 | 18 | 0 | 30 | 23 | 108 | 31 | 0 | 162 | 21 | 6 | 5 | 0 | 32 | 350 | |
| 12:45 PM | 12 | 112 | 2 | 0 | 126 | 8 | 6 | 16 | 0 | 30 | 22 | 126 | 20 | 0 | 168 | 22 | 4 | 6 | 0 | 32 | 356 | |
| Hourly Total | 36 | 442 | 15 | 0 | 493 | 19 | 25 | 69 | 0 | 113 | 81 | 436 | 89 | 0 | 606 | 86 | 18 | 32 | 0 | 136 | 1348 | |
| 1:00 PM | 9 | 87 | 7 | 0 | 103 | 4 | 1 | 17 | 0 | 22 | 24 | 117 | 18 | 0 | 159 | 18 | 2 | 13 | 0 | 33 | 317 | |
| 1:15 PM | 14 | 88 | 9 | 0 | 111 | 5 | 5 | 26 | 0 | 36 | 12 | 114 | 19 | 0 | 145 | 16 | 6 | 16 | 0 | 38 | 330 | |
| 1:30 PM | 17 | 123 | 5 | 0 | 145 | 7 | 6 | 13 | 0 | 26 | 18 | 117 | 11 | 0 | 146 | 23 | 1 | 15 | 0 | 39 | 356 | |
| 1:45 PM | 5 | 80 | 6 | 0 | 91 | 3 | 4 | 11 | 0 | 18 | 18 | 120 | 16 | 0 | 154 | 18 | 6 | 14 | 0 | 38 | 301 | |
| Hourly Total | 45 | 378 | 27 | 0 | 450 | 19 | 16 | 67 | 0 | 102 | 72 | 468 | 64 | 0 | 604 | 75 | 15 | 58 | 0 | 148 | 1304 | |
| 2:00 PM | 8 | 104 | 6 | 0 | 118 | 7 | 9 | 28 | 0 | 44 | 20 | 132 | 22 | 0 | 174 | 11 | 4 | 10 | 0 | 25 | 361 | |
| 2:15 PM | 14 | 98 | 3 | 0 | 115 | 7 | 6 | 17 | 0 | 30 | 23 | 129 | 30 | 0 | 182 | 17 | 8 | 10 | 0 | 35 | 362 | |
| 2:30 PM | 10 | 109 | 8 | 0 | 127 | 5 | 7 | 26 | 0 | 38 | 16 | 131 | 32 | 0 | 179 | 31 | 7 | 9 | 0 | 47 | 391 | |
| 2:45 PM | 6 | 115 | 5 | 0 | 126 | 4 | 2 | 23 | 0 | 29 | 18 | 120 | 14 | 0 | 152 | 23 | 5 | 6 | 0 | 34 | 341 | |

| Hourly Total | 38 | 426 | 22 | 0 | 486 | 23 | 24 | 94 | 0 | 141 | 77 | 512 | 98 | 0 | 687 | 82 | 24 | 35 | 0 | 141 | 1455 |
|----------------------|------|------|------|-----|------|------|------|------|-----|------|------|------|------|-----|------|------|------|------|-----|------|-------|
| 3:00 PM | 12 | 106 | 5 | 0 | 123 | 2 | 5 | 16 | 0 | 23 | 25 | 141 | 35 | 0 | 201 | 14 | 3 | 17 | 0 | 34 | 381 |
| 3:15 PM | 10 | 86 | 2 | 0 | 98 | 7 | 13 | 25 | 0 | 45 | 30 | 175 | 29 | 0 | 234 | 23 | 6 | 12 | 0 | 41 | 418 |
| 3:30 PM | 17 | 106 | 3 | 0 | 126 | 9 | 13 | 29 | 0 | 51 | 31 | 169 | 38 | 0 | 238 | 30 | 4 | 17 | 0 | 51 | 466 |
| 3:45 PM | 18 | 85 | 6 | 0 | 109 | 14 | 8 | 18 | 0 | 40 | 18 | 174 | 46 | 0 | 238 | 33 | 7 | 25 | 0 | 65 | 452 |
| Hourly Total | 57 | 383 | 16 | 0 | 456 | 32 | 39 | 88 | 0 | 159 | 104 | 659 | 148 | 0 | 911 | 100 | 20 | 71 | 0 | 191 | 1717 |
| 4:00 PM | 17 | 107 | 8 | 0 | 132 | 19 | 9 | 21 | 0 | 49 | 24 | 187 | 28 | 0 | 239 | 18 | 11 | 21 | 0 | 50 | 470 |
| 4:15 PM | 18 | 69 | 10 | 0 | 97 | 17 | 14 | 27 | 0 | 58 | 20 | 189 | 35 | 0 | 244 | 28 | 10 | 23 | 0 | 61 | 460 |
| 4:30 PM | 26 | 115 | 7 | 0 | 148 | 29 | 14 | 22 | 0 | 65 | 18 | 203 | 18 | 0 | 239 | 34 | 8 | 40 | 0 | 82 | 534 |
| 4:45 PM | 25 | 107 | 3 | 0 | 135 | 26 | 19 | 20 | 0 | 65 | 17 | 207 | 44 | 0 | 268 | 23 | 10 | 18 | 0 | 51 | 519 |
| Hourly Total | 86 | 398 | 28 | 0 | 512 | 91 | 56 | 90 | 0 | 237 | 79 | 786 | 125 | 0 | 990 | 103 | 39 | 102 | 0 | 244 | 1983 |
| 5:00 PM | 15 | 107 | 5 | 0 | 127 | 9 | 16 | 21 | 0 | 46 | 25 | 220 | 24 | 0 | 269 | 25 | 13 | 15 | 0 | 53 | 495 |
| 5:15 PM | 17 | 97 | 4 | 0 | 118 | 17 | 19 | 21 | 0 | 57 | 21 | 200 | 43 | 0 | 264 | 28 | 13 | 28 | 0 | 69 | 508 |
| 5:30 PM | 21 | 112 | 5 | 0 | 138 | 20 | 12 | 24 | 0 | 56 | 23 | 208 | 27 | 0 | 258 | 25 | 7 | 23 | 0 | 55 | 507 |
| 5:45 PM | 14 | 106 | 4 | 0 | 124 | 12 | 13 | 27 | 0 | 52 | 19 | 185 | 50 | 0 | 254 | 27 | 4 | 23 | 0 | 54 | 484 |
| Hourly Total | 67 | 422 | 18 | 0 | 507 | 58 | 60 | 93 | 0 | 211 | 88 | 813 | 144 | 0 | 1045 | 105 | 37 | 89 | 0 | 231 | 1994 |
| 6:00 PM | 11 | 83 | 4 | 0 | 98 | 7 | 10 | 19 | 0 | 36 | 24 | 138 | 40 | 0 | 202 | 37 | 10 | 27 | 0 | 74 | 410 |
| 6:15 PM | 18 | 133 | 4 | 0 | 155 | 14 | 6 | 16 | 0 | 36 | 20 | 139 | 29 | 0 | 188 | 23 | 8 | 17 | 0 | 48 | 427 |
| 6:30 PM | 19 | 114 | 5 | 0 | 138 | 3 | 6 | 15 | 0 | 24 | 22 | 110 | 34 | 0 | 166 | 38 | 6 | 17 | 0 | 61 | 389 |
| 6:45 PM | 10 | 93 | 4 | 0 | 107 | 5 | 8 | 12 | 0 | 25 | 17 | 116 | 45 | 0 | 178 | 20 | 7 | 18 | 0 | 45 | 355 |
| Hourly Total | 58 | 423 | 17 | 0 | 498 | 29 | 30 | 62 | 0 | 121 | 83 | 503 | 148 | 0 | 734 | 118 | 31 | 79 | 0 | 228 | 1581 |
| Grand Total | 618 | 5605 | 244 | 0 | 6467 | 358 | 371 | 1068 | 0 | 1797 | 890 | 5742 | 1123 | 0 | 7755 | 1207 | 288 | 694 | 0 | 2189 | 18208 |
| Approach % | 9.6 | 86.7 | 3.8 | 0.0 | - | 19.9 | 20.6 | 59.4 | 0.0 | - | 11.5 | 74.0 | 14.5 | 0.0 | - | 55.1 | 13.2 | 31.7 | 0.0 | - | - |
| Total % | 3.4 | 30.8 | 1.3 | 0.0 | 35.5 | 2.0 | 2.0 | 5.9 | 0.0 | 9.9 | 4.9 | 31.5 | 6.2 | 0.0 | 42.6 | 6.6 | 1.6 | 3.8 | 0.0 | 12.0 | - |
| Motorcycles | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 1 | 6 |
| % Motorcycles | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.3 | 0.0 | - | 0.1 | 0.1 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.1 | - | 0.0 | 0.0 |
| Cars & Light Goods | 596 | 5341 | 237 | 0 | 6174 | 348 | 360 | 1027 | 0 | 1735 | 851 | 5437 | 1081 | 0 | 7369 | 1165 | 282 | 677 | 0 | 2124 | 17402 |
| % Cars & Light Goods | 96.4 | 95.3 | 97.1 | - | 95.5 | 97.2 | 97.0 | 96.2 | - | 96.5 | 95.6 | 94.7 | 96.3 | - | 95.0 | 96.5 | 97.9 | 97.6 | - | 97.0 | 95.6 |
| Buses | 1 | 42 | 2 | 0 | 45 | 6 | 8 | 32 | 0 | 46 | 30 | 54 | 7 | 0 | 91 | 8 | 4 | 4 | 0 | 16 | 198 |
| % Buses | 0.2 | 0.7 | 0.8 | - | 0.7 | 1.7 | 2.2 | 3.0 | - | 2.6 | 3.4 | 0.9 | 0.6 | - | 1.2 | 0.7 | 1.4 | 0.6 | - | 0.7 | 1.1 |
| Single-Unit Trucks | 18 | 180 | 5 | 0 | 203 | 3 | 2 | 9 | 0 | 14 | 8 | 210 | 35 | 0 | 253 | 34 | 2 | 12 | 0 | 48 | 518 |
| % Single-Unit Trucks | 2.9 | 3.2 | 2.0 | - | 3.1 | 0.8 | 0.5 | 0.8 | - | 0.8 | 0.9 | 3.7 | 3.1 | - | 3.3 | 2.8 | 0.7 | 1.7 | - | 2.2 | 2.8 |
| Articulated Trucks | 3 | 41 | 0 | 0 | 44 | 1 | 0 | 0 | 0 | 1 | 0 | 39 | 0 | 0 | 39 | 0 | 0 | 0 | 0 | 0 | 84 |
| % Articulated Trucks | 0.5 | 0.7 | 0.0 | - | 0.7 | 0.3 | 0.0 | 0.0 | - | 0.1 | 0.0 | 0.7 | 0.0 | - | 0.5 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.5 |

Halifax Regional Municipality (Dartmouth, NS)
PO Box 1749

Halifax, Nova Scotia, Canada B3J 3A5
(902) 490-4866

Count Name: 22RQ704
Site Code: Beaver Bank Rd at Millwood Dr and
Stokil Dr
Start Date: 11/01/2022
Page No: 3



Turning Movement Data Plot

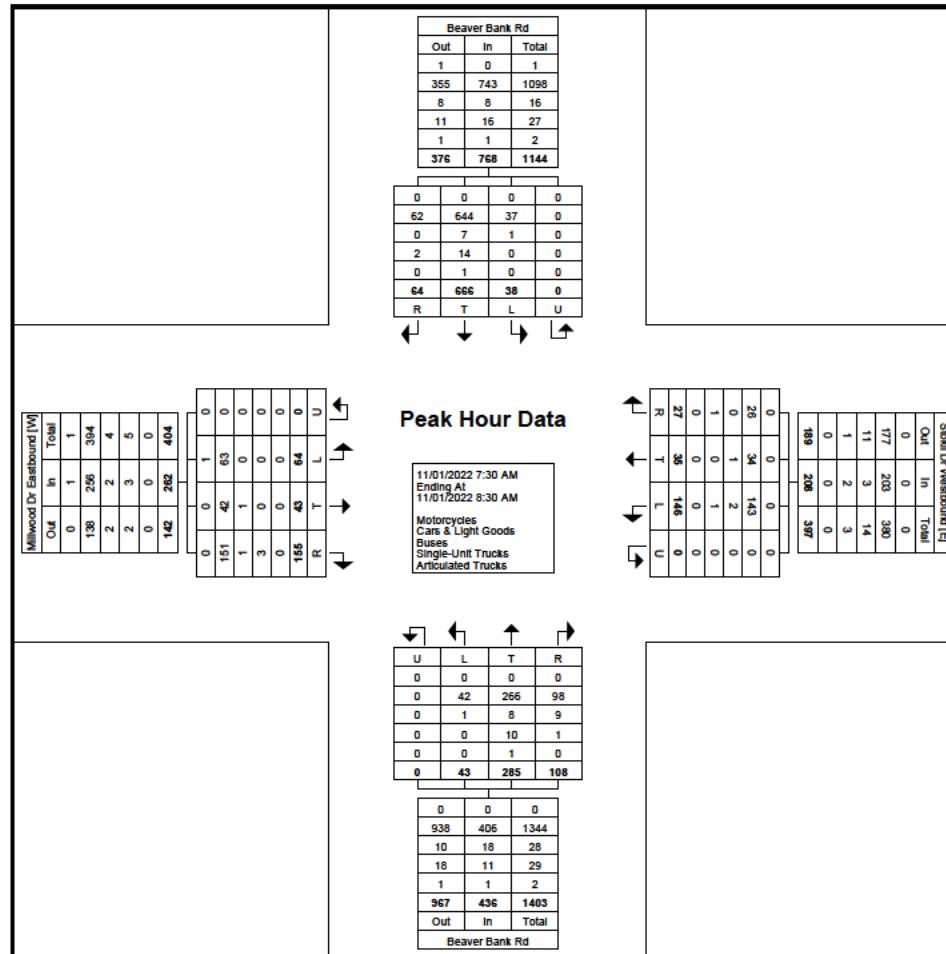
Turning Movement Peak Hour Data (7:30 AM)

| Start Time | Beaver Bank Rd Southbound | | | | | Stokil Dr Westbound | | | | | Beaver Bank Rd Northbound | | | | | Millwood Dr Eastbound | | | | | Int. Total | |
|----------------------|---------------------------|-------|-------|--------|------------|---------------------|-------|-------|--------|------------|---------------------------|-------|-------|--------|------------|-----------------------|-------|-------|--------|------------|------------|--|
| | Southbound | | | | | Westbound | | | | | Northbound | | | | | Eastbound | | | | | | |
| | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | | |
| 7:30 AM | 15 | 192 | 5 | 0 | 212 | 10 | 9 | 34 | 0 | 53 | 26 | 73 | 8 | 0 | 107 | 36 | 6 | 17 | 0 | 59 | 431 | |
| 7:45 AM | 16 | 164 | 10 | 0 | 190 | 5 | 8 | 33 | 0 | 46 | 29 | 64 | 13 | 0 | 106 | 38 | 10 | 13 | 0 | 61 | 403 | |
| 8:00 AM | 24 | 171 | 14 | 0 | 209 | 7 | 10 | 42 | 0 | 59 | 25 | 69 | 10 | 0 | 104 | 46 | 14 | 20 | 0 | 80 | 452 | |
| 8:15 AM | 9 | 139 | 9 | 0 | 157 | 5 | 8 | 37 | 0 | 50 | 28 | 79 | 12 | 0 | 119 | 35 | 13 | 14 | 0 | 62 | 388 | |
| Total | 64 | 666 | 38 | 0 | 768 | 27 | 35 | 146 | 0 | 208 | 108 | 285 | 43 | 0 | 436 | 155 | 43 | 64 | 0 | 262 | 1674 | |
| Approach % | 8.3 | 86.7 | 4.9 | 0.0 | - | 13.0 | 16.8 | 70.2 | 0.0 | - | 24.8 | 65.4 | 9.9 | 0.0 | - | 59.2 | 16.4 | 24.4 | 0.0 | - | - | |
| Total % | 3.8 | 39.8 | 2.3 | 0.0 | 45.9 | 1.6 | 2.1 | 8.7 | 0.0 | 12.4 | 6.5 | 17.0 | 2.6 | 0.0 | 26.0 | 9.3 | 2.6 | 3.8 | 0.0 | 15.7 | - | |
| PHF | 0.667 | 0.867 | 0.679 | 0.000 | 0.906 | 0.675 | 0.875 | 0.869 | 0.000 | 0.881 | 0.931 | 0.902 | 0.827 | 0.000 | 0.916 | 0.842 | 0.768 | 0.800 | 0.000 | 0.819 | 0.926 | |
| Motorcycles | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | |
| % Motorcycles | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 1.6 | - | 0.4 | 0.1 | |
| Cars & Light Goods | 62 | 644 | 37 | 0 | 743 | 26 | 34 | 143 | 0 | 203 | 98 | 266 | 42 | 0 | 406 | 151 | 42 | 63 | 0 | 256 | 1608 | |
| % Cars & Light Goods | 96.9 | 96.7 | 97.4 | - | 96.7 | 96.3 | 97.1 | 97.9 | - | 97.6 | 90.7 | 93.3 | 97.7 | - | 93.1 | 97.4 | 97.7 | 98.4 | - | 97.7 | 96.1 | |
| Buses | 0 | 7 | 1 | 0 | 8 | 0 | 1 | 2 | 0 | 3 | 9 | 8 | 1 | 0 | 18 | 1 | 1 | 0 | 0 | 2 | 31 | |
| % Buses | 0.0 | 1.1 | 2.6 | - | 1.0 | 0.0 | 2.9 | 1.4 | - | 1.4 | 8.3 | 2.8 | 2.3 | - | 4.1 | 0.6 | 2.3 | 0.0 | - | 0.8 | 1.9 | |
| Single-Unit Trucks | 2 | 14 | 0 | 0 | 16 | 1 | 0 | 1 | 0 | 2 | 1 | 10 | 0 | 0 | 11 | 3 | 0 | 0 | 0 | 3 | 32 | |
| % Single-Unit Trucks | 3.1 | 2.1 | 0.0 | - | 2.1 | 3.7 | 0.0 | 0.7 | - | 1.0 | 0.9 | 3.5 | 0.0 | - | 2.5 | 1.9 | 0.0 | 0.0 | - | 1.1 | 1.9 | |
| Articulated Trucks | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | |
| % Articulated Trucks | 0.0 | 0.2 | 0.0 | - | 0.1 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.4 | 0.0 | - | 0.2 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 | |

Halifax Regional Municipality (Dartmouth, NS)
PO Box 1749

Halifax, Nova Scotia, Canada B3J 3A5
(902) 490-4866

Count Name: 22RQ704
Site Code: Beaver Bank Rd at Millwood Dr and
Stokil Dr
Start Date: 11/01/2022
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Turning Movement Peak Hour Data Plot (7:30 AM)

Halifax Regional Municipality (Dartmouth, NS)
PO Box 1749

Halifax, Nova Scotia, Canada B3J 3A5
(902) 490-4866

Count Name: 22RQ704
Site Code: Beaver Bank Rd at Millwood Dr and Stokil Dr
Start Date: 11/01/2022
Page No: 6

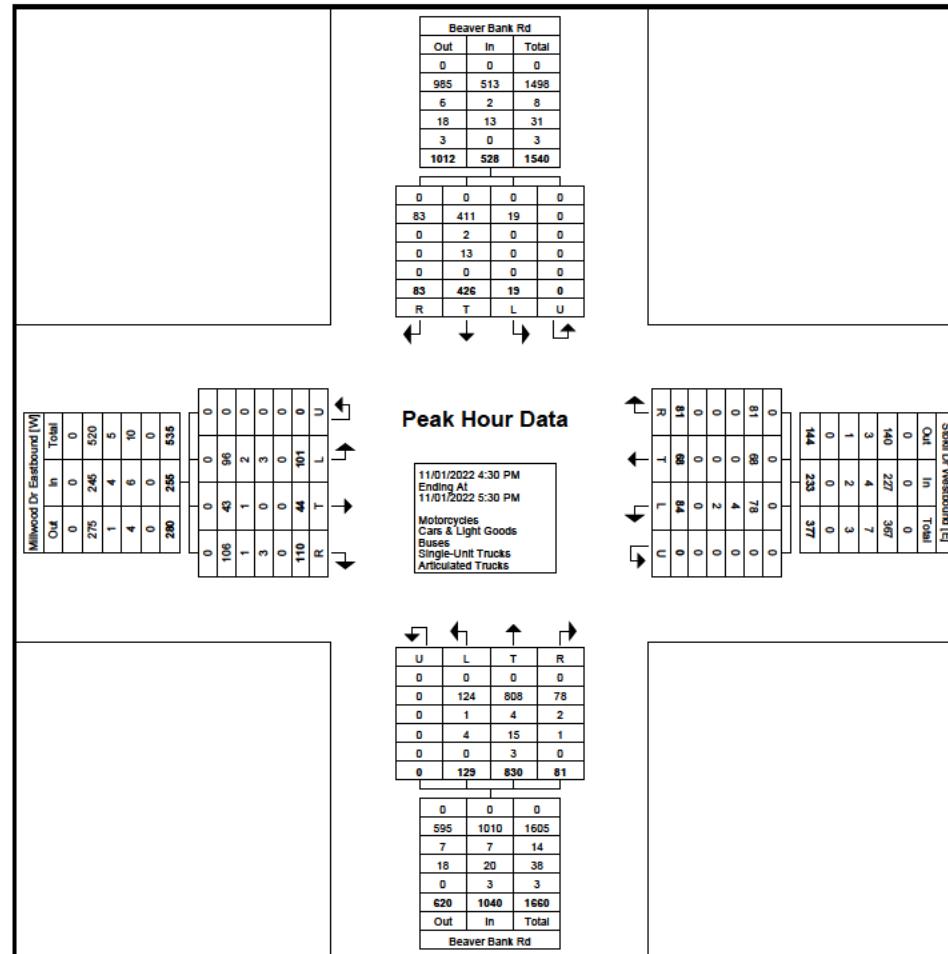
Turning Movement Peak Hour Data (4:30 PM)

| Start Time | Beaver Bank Rd Southbound | | | | | Stokil Dr Westbound | | | | | Beaver Bank Rd Northbound | | | | | Millwood Dr Eastbound | | | | | Int. Total | |
|----------------------|---------------------------|-------|-------|--------|------------|---------------------|-------|-------|--------|------------|---------------------------|-------|-------|--------|------------|-----------------------|-------|-------|--------|------------|------------|--|
| | Southbound | | | | | Westbound | | | | | Northbound | | | | | Eastbound | | | | | | |
| | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | | |
| 4:30 PM | 26 | 115 | 7 | 0 | 148 | 29 | 14 | 22 | 0 | 65 | 18 | 203 | 18 | 0 | 239 | 34 | 8 | 40 | 0 | 82 | 534 | |
| 4:45 PM | 25 | 107 | 3 | 0 | 135 | 26 | 19 | 20 | 0 | 65 | 17 | 207 | 44 | 0 | 268 | 23 | 10 | 18 | 0 | 51 | 519 | |
| 5:00 PM | 15 | 107 | 5 | 0 | 127 | 9 | 16 | 21 | 0 | 46 | 25 | 220 | 24 | 0 | 269 | 25 | 13 | 15 | 0 | 53 | 495 | |
| 5:15 PM | 17 | 97 | 4 | 0 | 118 | 17 | 19 | 21 | 0 | 57 | 21 | 200 | 43 | 0 | 264 | 28 | 13 | 28 | 0 | 69 | 508 | |
| Total | 83 | 426 | 19 | 0 | 528 | 81 | 68 | 84 | 0 | 233 | 81 | 830 | 129 | 0 | 1040 | 110 | 44 | 101 | 0 | 255 | 2056 | |
| Approach % | 15.7 | 80.7 | 3.6 | 0.0 | - | 34.8 | 29.2 | 36.1 | 0.0 | - | 7.8 | 79.8 | 12.4 | 0.0 | - | 43.1 | 17.3 | 39.6 | 0.0 | - | - | |
| Total % | 4.0 | 20.7 | 0.9 | 0.0 | 25.7 | 3.9 | 3.3 | 4.1 | 0.0 | 11.3 | 3.9 | 40.4 | 6.3 | 0.0 | 50.6 | 5.4 | 2.1 | 4.9 | 0.0 | 12.4 | - | |
| PHF | 0.798 | 0.926 | 0.679 | 0.000 | 0.892 | 0.698 | 0.895 | 0.955 | 0.000 | 0.896 | 0.810 | 0.943 | 0.733 | 0.000 | 0.967 | 0.809 | 0.846 | 0.631 | 0.000 | 0.777 | 0.963 | |
| Motorcycles | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| % Motorcycles | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | |
| Cars & Light Goods | 83 | 411 | 19 | 0 | 513 | 81 | 68 | 78 | 0 | 227 | 78 | 808 | 124 | 0 | 1010 | 106 | 43 | 96 | 0 | 245 | 1995 | |
| % Cars & Light Goods | 100.0 | 96.5 | 100.0 | - | 97.2 | 100.0 | 100.0 | 92.9 | - | 97.4 | 96.3 | 97.3 | 96.1 | - | 97.1 | 96.4 | 97.7 | 95.0 | - | 96.1 | 97.0 | |
| Buses | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 4 | 0 | 4 | 2 | 4 | 1 | 0 | 7 | 1 | 1 | 2 | 0 | 4 | 17 | |
| % Buses | 0.0 | 0.5 | 0.0 | - | 0.4 | 0.0 | 0.0 | 4.8 | - | 1.7 | 2.5 | 0.5 | 0.8 | - | 0.7 | 0.9 | 2.3 | 2.0 | - | 1.6 | 0.8 | |
| Single-Unit Trucks | 0 | 13 | 0 | 0 | 13 | 0 | 0 | 2 | 0 | 2 | 1 | 15 | 4 | 0 | 20 | 3 | 0 | 3 | 0 | 6 | 41 | |
| % Single-Unit Trucks | 0.0 | 3.1 | 0.0 | - | 2.5 | 0.0 | 0.0 | 2.4 | - | 0.9 | 1.2 | 1.8 | 3.1 | - | 1.9 | 2.7 | 0.0 | 3.0 | - | 2.4 | 2.0 | |
| Articulated Trucks | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 3 | |
| % Articulated Trucks | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.4 | 0.0 | - | 0.3 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 | |

Halifax Regional Municipality (Dartmouth, NS)
PO Box 1749

Halifax, Nova Scotia, Canada B3J 3A5
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Count Name: 22RQ704
Site Code: Beaver Bank Rd at Millwood Dr and
Stokil Dr
Start Date: 11/01/2022
Page No: 7



Turning Movement Peak Hour Data Plot (4:30 PM)

Turning Movement Data

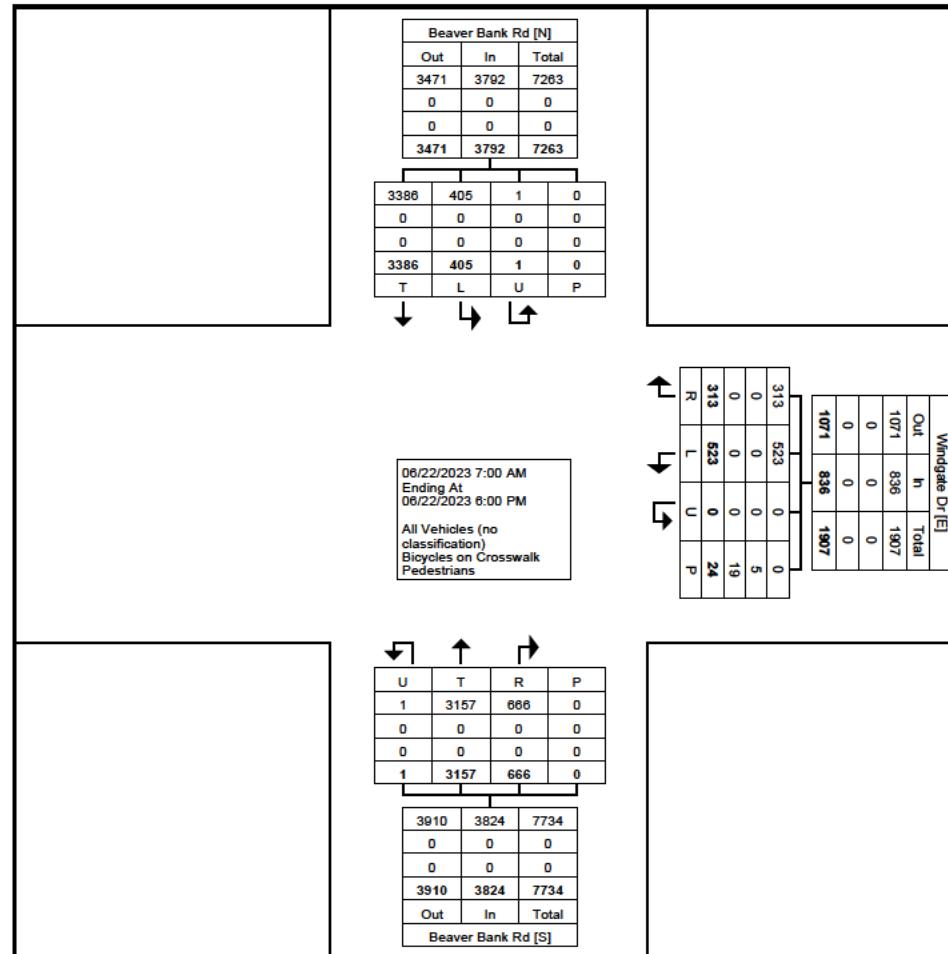
| Start Time | Beaver Bank Rd Southbound | | | | | Windgate Dr Westbound | | | | | Beaver Bank Rd Northbound | | | | | Int. Total |
|------------------------------------|------------------------------|-------|--------|------|------------|--------------------------|-------|--------|------|------------|------------------------------|-------|--------|-------|------------|------------|
| | Thru | Left | U-Turn | Peds | App. Total | Right | Left | U-Turn | Peds | App. Total | Right | Thru | U-Turn | Peds | App. Total | |
| 7:00 AM | 196 | 21 | 0 | 0 | 217 | 9 | 12 | 0 | 3 | 21 | 17 | 50 | 0 | 0 | 67 | 305 |
| 7:15 AM | 191 | 21 | 1 | 0 | 213 | 9 | 16 | 0 | 0 | 25 | 28 | 94 | 0 | 0 | 122 | 360 |
| 7:30 AM | 223 | 24 | 0 | 0 | 247 | 12 | 25 | 0 | 0 | 37 | 22 | 96 | 0 | 0 | 118 | 402 |
| 7:45 AM | 208 | 40 | 0 | 0 | 248 | 10 | 12 | 0 | 2 | 22 | 19 | 89 | 0 | 0 | 108 | 378 |
| Hourly Total | 818 | 106 | 1 | 0 | 925 | 40 | 65 | 0 | 5 | 105 | 86 | 329 | 0 | 0 | 415 | 1445 |
| 8:00 AM | 167 | 23 | 0 | 0 | 190 | 4 | 16 | 0 | 0 | 20 | 21 | 75 | 0 | 0 | 96 | 306 |
| 8:15 AM | 161 | 16 | 0 | 0 | 177 | 7 | 21 | 0 | 2 | 28 | 19 | 80 | 0 | 0 | 99 | 304 |
| 8:30 AM | 184 | 18 | 0 | 0 | 202 | 6 | 18 | 0 | 1 | 24 | 21 | 85 | 0 | 0 | 106 | 332 |
| 8:45 AM | 148 | 27 | 0 | 0 | 175 | 4 | 18 | 0 | 0 | 22 | 27 | 71 | 0 | 0 | 98 | 295 |
| Hourly Total | 660 | 84 | 0 | 0 | 744 | 21 | 73 | 0 | 3 | 94 | 88 | 311 | 0 | 0 | 399 | 1237 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 11:00 AM | 88 | 11 | 0 | 0 | 99 | 6 | 30 | 0 | 1 | 36 | 20 | 93 | 0 | 0 | 113 | 248 |
| 11:15 AM | 116 | 13 | 0 | 0 | 129 | 16 | 22 | 0 | 0 | 38 | 19 | 77 | 0 | 0 | 96 | 263 |
| 11:30 AM | 110 | 18 | 0 | 0 | 128 | 17 | 15 | 0 | 2 | 32 | 28 | 109 | 0 | 0 | 137 | 297 |
| 11:45 AM | 115 | 16 | 0 | 0 | 131 | 11 | 22 | 0 | 0 | 33 | 24 | 120 | 0 | 0 | 144 | 308 |
| Hourly Total | 429 | 58 | 0 | 0 | 487 | 50 | 89 | 0 | 3 | 139 | 91 | 399 | 0 | 0 | 490 | 1116 |
| 12:00 PM | 115 | 15 | 0 | 0 | 130 | 10 | 29 | 0 | 2 | 39 | 28 | 120 | 0 | 0 | 148 | 317 |
| 12:15 PM | 93 | 13 | 0 | 0 | 106 | 9 | 16 | 0 | 1 | 25 | 20 | 137 | 0 | 0 | 157 | 288 |
| 12:30 PM | 115 | 13 | 0 | 0 | 128 | 11 | 23 | 0 | 0 | 34 | 32 | 110 | 0 | 0 | 142 | 304 |
| 12:45 PM | 102 | 14 | 0 | 0 | 116 | 13 | 16 | 0 | 0 | 29 | 20 | 97 | 0 | 0 | 117 | 262 |
| Hourly Total | 425 | 55 | 0 | 0 | 480 | 43 | 84 | 0 | 3 | 127 | 100 | 464 | 0 | 0 | 564 | 1171 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 4:00 PM | 122 | 10 | 0 | 0 | 132 | 27 | 25 | 0 | 1 | 52 | 26 | 210 | 0 | 0 | 236 | 420 |
| 4:15 PM | 134 | 17 | 0 | 0 | 151 | 14 | 28 | 0 | 1 | 42 | 46 | 204 | 0 | 0 | 250 | 443 |
| 4:30 PM | 118 | 7 | 0 | 0 | 125 | 26 | 25 | 0 | 1 | 51 | 32 | 204 | 0 | 0 | 236 | 412 |
| 4:45 PM | 126 | 13 | 0 | 0 | 139 | 12 | 24 | 0 | 2 | 36 | 35 | 225 | 0 | 0 | 260 | 435 |
| Hourly Total | 500 | 47 | 0 | 0 | 547 | 79 | 102 | 0 | 5 | 181 | 139 | 843 | 0 | 0 | 982 | 1710 |
| 5:00 PM | 122 | 16 | 0 | 0 | 138 | 25 | 29 | 0 | 0 | 54 | 41 | 218 | 0 | 0 | 259 | 451 |
| 5:15 PM | 128 | 8 | 0 | 0 | 136 | 24 | 32 | 0 | 0 | 56 | 48 | 219 | 1 | 0 | 268 | 460 |
| 5:30 PM | 165 | 12 | 0 | 0 | 177 | 21 | 22 | 0 | 1 | 43 | 41 | 178 | 0 | 0 | 219 | 439 |
| 5:45 PM | 139 | 19 | 0 | 0 | 158 | 10 | 27 | 0 | 4 | 37 | 32 | 196 | 0 | 0 | 228 | 423 |
| Hourly Total | 554 | 55 | 0 | 0 | 609 | 80 | 110 | 0 | 5 | 190 | 162 | 811 | 1 | 0 | 974 | 1773 |
| Grand Total | 3386 | 405 | 1 | 0 | 3792 | 313 | 523 | 0 | 24 | 836 | 666 | 3157 | 1 | 0 | 3824 | 8452 |
| Approach % | 89.3 | 10.7 | 0.0 | - | - | 37.4 | 62.6 | 0.0 | - | - | 17.4 | 82.6 | 0.0 | - | - | - |
| Total % | 40.1 | 4.8 | 0.0 | - | 44.9 | 3.7 | 6.2 | 0.0 | - | 9.9 | 7.9 | 37.4 | 0.0 | - | 45.2 | - |
| All Vehicles (no classification) | 3386 | 405 | 1 | - | 3792 | 313 | 523 | 0 | - | 836 | 666 | 3157 | 1 | - | 3824 | 8452 |
| % All Vehicles (no classification) | 100.0 | 100.0 | 100.0 | - | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | 100.0 | 100.0 | 100.0 |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 5 | - | - | - | - | 0 | - | - |

| | | | | | | | | | | | | | |
|-------------------------|---|---|---|---|---|---|------|---|---|---|---|---|---|
| % Bicycles on Crosswalk | - | - | - | - | - | - | 20.8 | - | - | - | - | - | - |
| Pedestrians | - | - | - | 0 | - | - | 19 | - | - | - | 0 | - | - |
| % Pedestrians | - | - | - | - | - | - | 79.2 | - | - | - | - | - | - |

Halifax Regional Municipality (Dartmouth, NS)
PO Box 1749

Halifax, Nova Scotia, Canada B3J 3A5
(902) 490-4866

Count Name: 23RQ632
Site Code: Beaver Bank Rd at Windgate Dr
Start Date: 06/22/2023
Page No: 3



Turning Movement Data Plot

Halifax Regional Municipality (Dartmouth, NS)
PO Box 1749

Halifax, Nova Scotia, Canada B3J 3A5
(902) 490-4866

Count Name: 23RQ632
Site Code: Beaver Bank Rd at Windgate Dr
Start Date: 06/22/2023
Page No: 4

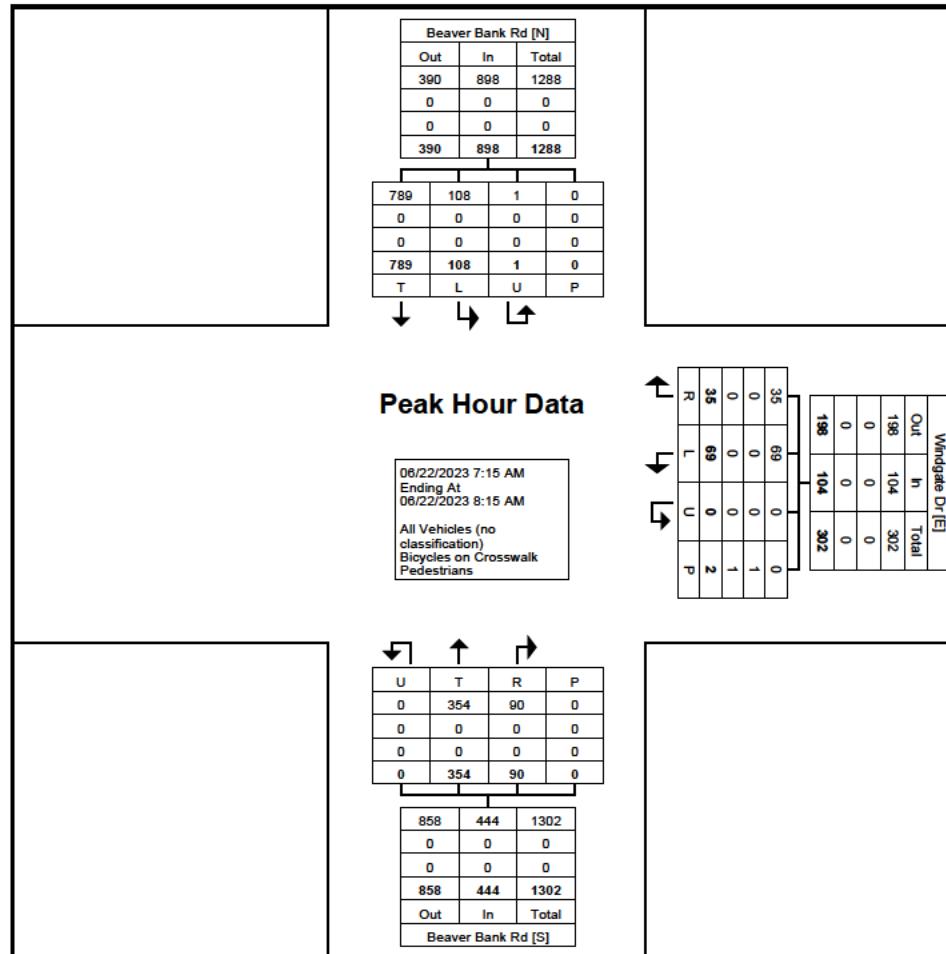
Turning Movement Peak Hour Data (7:15 AM)

| Start Time | Beaver Bank Rd Southbound | | | | | Windgate Dr Westbound | | | | | Beaver Bank Rd Northbound | | | | | Int. Total |
|------------------------------------|------------------------------|-------|--------|------|------------|--------------------------|-------|--------|------|------------|------------------------------|-------|--------|------|------------|------------|
| | Thru | Left | U-Turn | Peds | App. Total | Right | Left | U-Turn | Peds | App. Total | Right | Thru | U-Turn | Peds | App. Total | |
| 7:15 AM | 191 | 21 | 1 | 0 | 213 | 9 | 16 | 0 | 0 | 25 | 28 | 94 | 0 | 0 | 122 | 360 |
| 7:30 AM | 223 | 24 | 0 | 0 | 247 | 12 | 25 | 0 | 0 | 37 | 22 | 96 | 0 | 0 | 118 | 402 |
| 7:45 AM | 208 | 40 | 0 | 0 | 248 | 10 | 12 | 0 | 2 | 22 | 19 | 89 | 0 | 0 | 108 | 378 |
| 8:00 AM | 167 | 23 | 0 | 0 | 190 | 4 | 16 | 0 | 0 | 20 | 21 | 75 | 0 | 0 | 96 | 306 |
| Total | 789 | 108 | 1 | 0 | 898 | 35 | 69 | 0 | 2 | 104 | 90 | 354 | 0 | 0 | 444 | 1446 |
| Approach % | 87.9 | 12.0 | 0.1 | - | - | 33.7 | 66.3 | 0.0 | - | - | 20.3 | 79.7 | 0.0 | - | - | - |
| Total % | 54.6 | 7.5 | 0.1 | - | 62.1 | 2.4 | 4.8 | 0.0 | - | 7.2 | 6.2 | 24.5 | 0.0 | - | 30.7 | - |
| PHF | 0.885 | 0.675 | 0.250 | - | 0.905 | 0.729 | 0.690 | 0.000 | - | 0.703 | 0.804 | 0.922 | 0.000 | - | 0.910 | 0.899 |
| All Vehicles (no classification) | 789 | 108 | 1 | - | 898 | 35 | 69 | 0 | - | 104 | 90 | 354 | 0 | - | 444 | 1446 |
| % All Vehicles (no classification) | 100.0 | 100.0 | 100.0 | - | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - |
| % Bicycles on Crosswalk | - | - | - | - | - | - | - | - | 50.0 | - | - | - | - | - | - | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - |
| % Pedestrians | - | - | - | - | - | - | - | - | 50.0 | - | - | - | - | - | - | - |

Halifax Regional Municipality (Dartmouth, NS)
PO Box 1749

Halifax, Nova Scotia, Canada B3J 3A5
(902) 490-4866

Count Name: 23RQ632
Site Code: Beaver Bank Rd at Windgate Dr
Start Date: 06/22/2023
Page No: 5



Turning Movement Peak Hour Data Plot (7:15 AM)

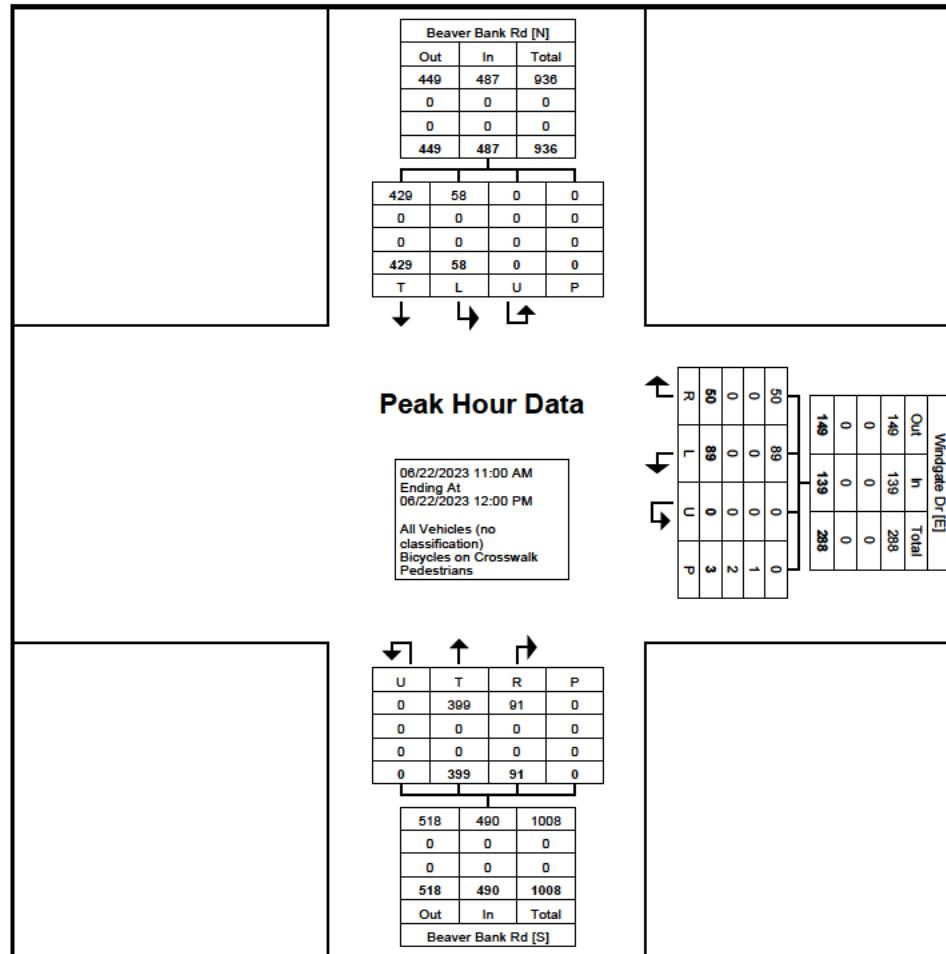
Turning Movement Peak Hour Data (11:00 AM)

| Start Time | Beaver Bank Rd Southbound | | | | | Windgate Dr Westbound | | | | | Beaver Bank Rd Northbound | | | | | Int. Total |
|------------------------------------|------------------------------|-------|--------|------|------------|--------------------------|-------|--------|------|------------|------------------------------|-------|--------|------|------------|------------|
| | Thru | Left | U-Turn | Peds | App. Total | Right | Left | U-Turn | Peds | App. Total | Right | Thru | U-Turn | Peds | App. Total | |
| 11:00 AM | 88 | 11 | 0 | 0 | 99 | 6 | 30 | 0 | 1 | 36 | 20 | 93 | 0 | 0 | 113 | 248 |
| 11:15 AM | 116 | 13 | 0 | 0 | 129 | 16 | 22 | 0 | 0 | 38 | 19 | 77 | 0 | 0 | 96 | 263 |
| 11:30 AM | 110 | 18 | 0 | 0 | 128 | 17 | 15 | 0 | 2 | 32 | 28 | 109 | 0 | 0 | 137 | 297 |
| 11:45 AM | 115 | 16 | 0 | 0 | 131 | 11 | 22 | 0 | 0 | 33 | 24 | 120 | 0 | 0 | 144 | 308 |
| Total | 429 | 58 | 0 | 0 | 487 | 50 | 89 | 0 | 3 | 139 | 91 | 399 | 0 | 0 | 490 | 1116 |
| Approach % | 88.1 | 11.9 | 0.0 | - | - | 36.0 | 64.0 | 0.0 | - | - | 18.6 | 81.4 | 0.0 | - | - | - |
| Total % | 38.4 | 5.2 | 0.0 | - | 43.6 | 4.5 | 8.0 | 0.0 | - | 12.5 | 8.2 | 35.8 | 0.0 | - | 43.9 | - |
| PHF | 0.925 | 0.806 | 0.000 | - | 0.929 | 0.735 | 0.742 | 0.000 | - | 0.914 | 0.813 | 0.831 | 0.000 | - | 0.851 | 0.906 |
| All Vehicles (no classification) | 429 | 58 | 0 | - | 487 | 50 | 89 | 0 | - | 139 | 91 | 399 | 0 | - | 490 | 1116 |
| % All Vehicles (no classification) | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - |
| % Bicycles on Crosswalk | - | - | - | - | - | - | - | - | 33.3 | - | - | - | - | - | - | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 2 | - | - | - | - | 0 | - | - |
| % Pedestrians | - | - | - | - | - | - | - | - | 66.7 | - | - | - | - | - | - | - |

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Turning Movement Peak Hour Data Plot (11:00 AM)

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Count Name: 23RQ632
Site Code: Beaver Bank Rd at Windgate Dr
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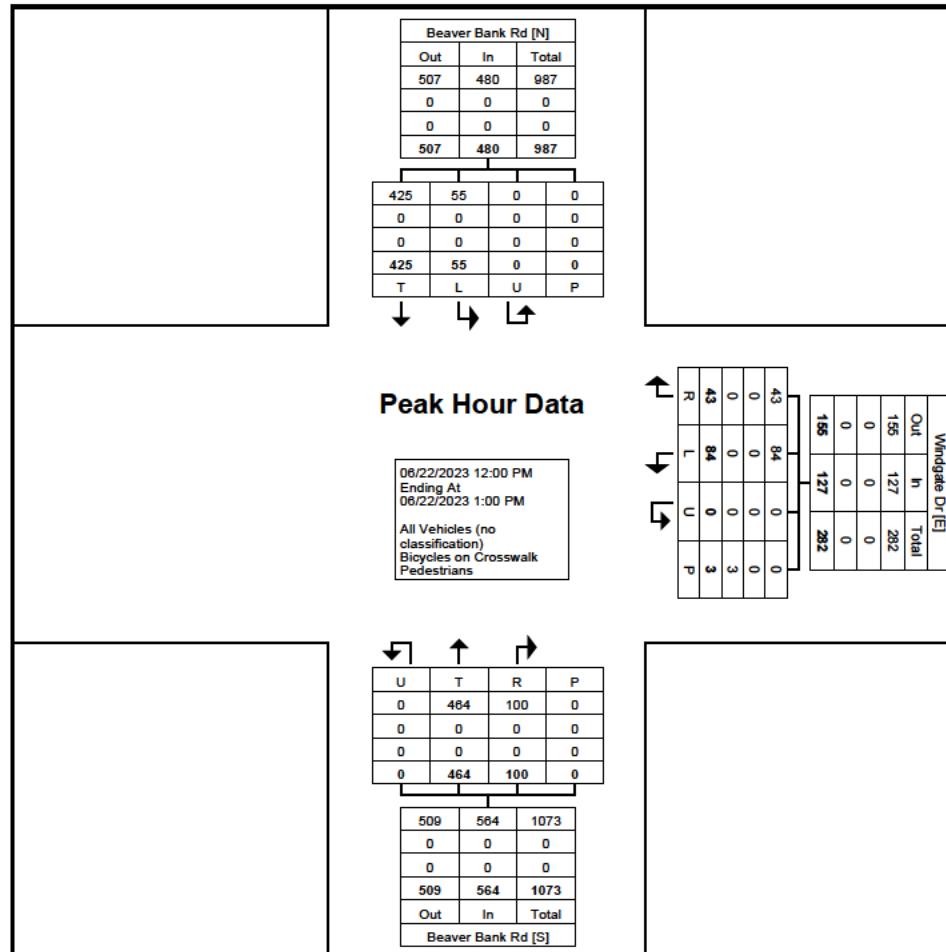
Turning Movement Peak Hour Data (12:00 PM)

| Start Time | Beaver Bank Rd Southbound | | | | | Windgate Dr Westbound | | | | | Beaver Bank Rd Northbound | | | | | Int. Total |
|------------------------------------|------------------------------|-------|--------|------|------------|--------------------------|-------|--------|-------|------------|------------------------------|-------|--------|------|------------|------------|
| | Thru | Left | U-Turn | Peds | App. Total | Right | Left | U-Turn | Peds | App. Total | Right | Thru | U-Turn | Peds | App. Total | |
| 12:00 PM | 115 | 15 | 0 | 0 | 130 | 10 | 29 | 0 | 2 | 39 | 28 | 120 | 0 | 0 | 148 | 317 |
| 12:15 PM | 93 | 13 | 0 | 0 | 106 | 9 | 16 | 0 | 1 | 25 | 20 | 137 | 0 | 0 | 157 | 288 |
| 12:30 PM | 115 | 13 | 0 | 0 | 128 | 11 | 23 | 0 | 0 | 34 | 32 | 110 | 0 | 0 | 142 | 304 |
| 12:45 PM | 102 | 14 | 0 | 0 | 116 | 13 | 16 | 0 | 0 | 29 | 20 | 97 | 0 | 0 | 117 | 262 |
| Total | 425 | 55 | 0 | 0 | 480 | 43 | 84 | 0 | 3 | 127 | 100 | 464 | 0 | 0 | 564 | 1171 |
| Approach % | 88.5 | 11.5 | 0.0 | - | - | 33.9 | 66.1 | 0.0 | - | - | 17.7 | 82.3 | 0.0 | - | - | - |
| Total % | 36.3 | 4.7 | 0.0 | - | 41.0 | 3.7 | 7.2 | 0.0 | - | 10.8 | 8.5 | 39.6 | 0.0 | - | 48.2 | - |
| PHF | 0.924 | 0.917 | 0.000 | - | 0.923 | 0.827 | 0.724 | 0.000 | - | 0.814 | 0.781 | 0.847 | 0.000 | - | 0.898 | 0.924 |
| All Vehicles (no classification) | 425 | 55 | 0 | - | 480 | 43 | 84 | 0 | - | 127 | 100 | 464 | 0 | - | 564 | 1171 |
| % All Vehicles (no classification) | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| % Bicycles on Crosswalk | - | - | - | - | - | - | - | - | 0.0 | - | - | - | - | - | - | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 3 | - | - | - | - | 0 | - | - |
| % Pedestrians | - | - | - | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - |

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Turning Movement Peak Hour Data Plot (12:00 PM)

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Count Name: 23RQ632
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Start Date: 06/22/2023
Page No: 10

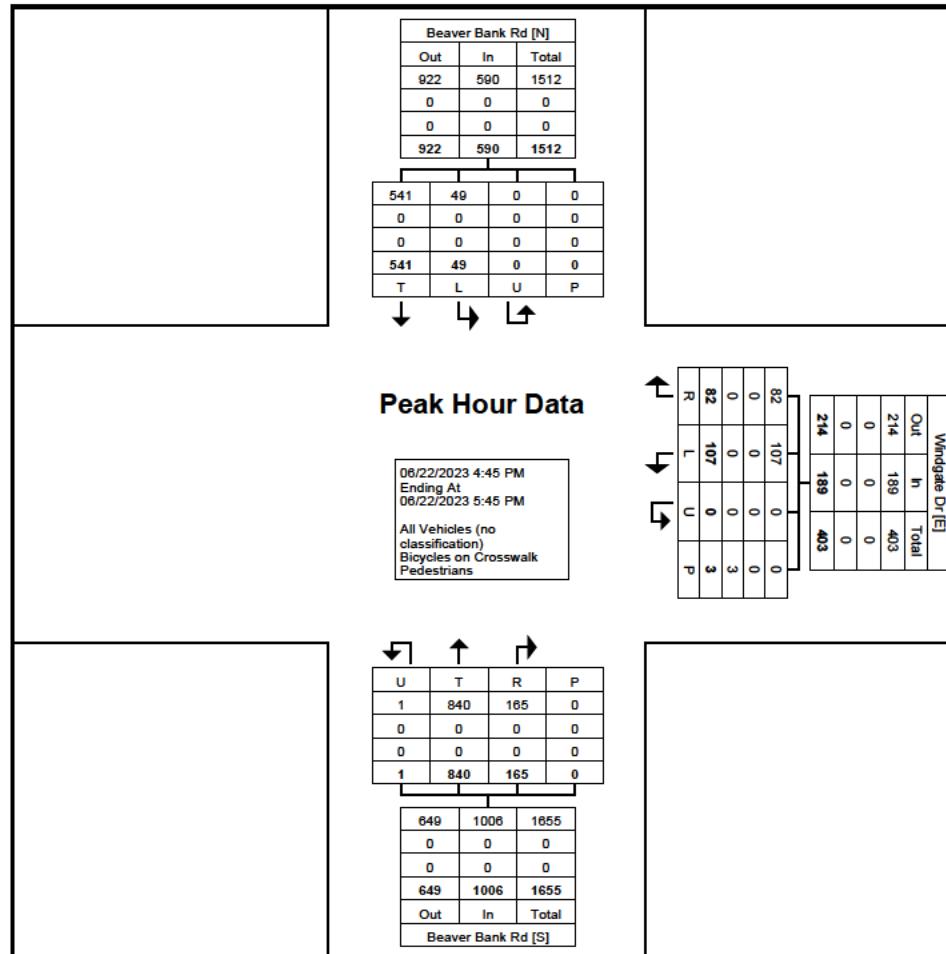
Turning Movement Peak Hour Data (4:45 PM)

| Start Time | Beaver Bank Rd Southbound | | | | | Windgate Dr Westbound | | | | | Beaver Bank Rd Northbound | | | | | Int. Total |
|------------------------------------|------------------------------|-------|--------|------|------------|--------------------------|-------|--------|-------|------------|------------------------------|-------|--------|------|------------|------------|
| | Thru | Left | U-Turn | Peds | App. Total | Right | Left | U-Turn | Peds | App. Total | Right | Thru | U-Turn | Peds | App. Total | |
| 4:45 PM | 126 | 13 | 0 | 0 | 139 | 12 | 24 | 0 | 2 | 36 | 35 | 225 | 0 | 0 | 260 | 435 |
| 5:00 PM | 122 | 16 | 0 | 0 | 138 | 25 | 29 | 0 | 0 | 54 | 41 | 218 | 0 | 0 | 259 | 451 |
| 5:15 PM | 128 | 8 | 0 | 0 | 136 | 24 | 32 | 0 | 0 | 56 | 48 | 219 | 1 | 0 | 268 | 460 |
| 5:30 PM | 165 | 12 | 0 | 0 | 177 | 21 | 22 | 0 | 1 | 43 | 41 | 178 | 0 | 0 | 219 | 439 |
| Total | 541 | 49 | 0 | 0 | 590 | 82 | 107 | 0 | 3 | 189 | 165 | 840 | 1 | 0 | 1006 | 1785 |
| Approach % | 91.7 | 8.3 | 0.0 | - | - | 43.4 | 56.6 | 0.0 | - | - | 16.4 | 83.5 | 0.1 | - | - | - |
| Total % | 30.3 | 2.7 | 0.0 | - | 33.1 | 4.6 | 6.0 | 0.0 | - | 10.6 | 9.2 | 47.1 | 0.1 | - | 56.4 | - |
| PHF | 0.820 | 0.766 | 0.000 | - | 0.833 | 0.820 | 0.836 | 0.000 | - | 0.844 | 0.859 | 0.933 | 0.250 | - | 0.938 | 0.970 |
| All Vehicles (no classification) | 541 | 49 | 0 | - | 590 | 82 | 107 | 0 | - | 189 | 165 | 840 | 1 | - | 1006 | 1785 |
| % All Vehicles (no classification) | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 | 100.0 | - | - | 100.0 | 100.0 |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| % Bicycles on Crosswalk | - | - | - | - | - | - | - | - | 0.0 | - | - | - | - | - | - | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 3 | - | - | - | - | 0 | - | - |
| % Pedestrians | - | - | - | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - |

Halifax Regional Municipality (Dartmouth, NS)
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Count Name: 23RQ632
Site Code: Beaver Bank Rd at Windgate Dr
Start Date: 06/22/2023
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Turning Movement Peak Hour Data Plot (4:45 PM)

APPENDIX B: EXISTING SYNCHRO REPORTS

Lanes, Volumes, Timings

Existing AM (2024)

1: Beaver Bank Road & Millwood Drive/Stokil Drive

10/09/2024

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|-----|-------|-------|-----|-------|------|-----|-------|--------|-----|
| Lane Configurations | ↑ | ↓ | | ↑ | ↓ | | ↑ | ↓ | | ↑ | ↓ | |
| Traffic Volume (vph) | 64 | 43 | 155 | 146 | 35 | 27 | 43 | 285 | 108 | 38 | 666 | 64 |
| Future Volume (vph) | 64 | 43 | 155 | 146 | 35 | 27 | 43 | 285 | 108 | 38 | 666 | 64 |
| Satd. Flow (prot) | 1789 | 1625 | 0 | 1789 | 1697 | 0 | 1789 | 1705 | 0 | 1772 | 1829 | 0 |
| Flt Permitted | 0.705 | | | | | | 0.103 | | | 0.426 | | |
| Satd. Flow (perm) | 1324 | 1625 | 0 | 483 | 1697 | 0 | 194 | 1705 | 0 | 794 | 1829 | 0 |
| Satd. Flow (RTOR) | | 113 | | | | 34 | | | 21 | | | 7 |
| Lane Group Flow (vph) | 80 | 241 | 0 | 168 | 80 | 0 | 52 | 433 | 0 | 56 | 862 | 0 |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 3 | 8 | | 7 | 4 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 8 | | | 4 | | | 6 | | | 2 | | |
| Total Split (s) | 12.0 | 31.2 | | 12.0 | 31.2 | | 16.0 | 71.4 | | 12.0 | 71.4 | |
| Total Lost Time (s) | 4.0 | 6.2 | | 4.0 | 6.2 | | 4.0 | 6.4 | | 4.0 | 6.4 | |
| Act Effct Green (s) | 24.3 | 14.0 | | 26.3 | 18.0 | | 63.9 | 56.1 | | 63.9 | 56.1 | |
| Actuated g/C Ratio | 0.23 | 0.13 | | 0.25 | 0.17 | | 0.61 | 0.54 | | 0.61 | 0.54 | |
| v/c Ratio | 0.23 | 0.76 | | 0.74 | 0.25 | | 0.22 | 0.47 | | 0.10 | 0.87 | |
| Control Delay (s/veh) | 34.4 | 41.2 | | 56.1 | 30.1 | | 9.6 | 17.0 | | 7.8 | 33.4 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay (s/veh) | 34.4 | 41.2 | | 56.1 | 30.1 | | 9.6 | 17.0 | | 7.8 | 33.4 | |
| LOS | C | D | | E | C | | A | B | | A | C | |
| Approach Delay (s/veh) | 39.5 | | | | 47.7 | | | 16.2 | | | 31.8 | |
| Approach LOS | D | | | | D | | | B | | | C | |
| Queue Length 50th (m) | 14.1 | 28.1 | | 31.2 | 9.4 | | 3.4 | 50.5 | | 3.7 | 148.8 | |
| Queue Length 95th (m) | 23.5 | 42.0 | | #58.2 | 22.8 | | 8.5 | 89.5 | | 7.3 | #253.0 | |
| Internal Link Dist (m) | | 142.5 | | | 100.7 | | | 85.0 | | | 195.0 | |
| Turn Bay Length (m) | 90.0 | | | 50.0 | | | 90.0 | | | 60.0 | | |
| Base Capacity (vph) | 352 | 495 | | 227 | 454 | | 317 | 1179 | | 570 | 1204 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.23 | 0.49 | | 0.74 | 0.18 | | 0.16 | 0.37 | | 0.10 | 0.72 | |

Intersection Summary

Cycle Length: 130.6

Actuated Cycle Length: 104.3

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.87

Intersection Signal Delay (s/veh): 31.2

Intersection LOS: C

Intersection Capacity Utilization 72.9%

ICU Level of Service C

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Beaver Bank Road & Millwood Drive/Stokil Drive



242101 Foxburrow TIS

Harbourside Transportation Consultants

Synchro 12 Report

| Intersection | | | | | | |
|----------------------------|--------|------------------------|-------|----------------------------|-------|--------------------------------|
| Int Delay, s/veh | 17.9 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | W | B | T | T | B | U |
| Traffic Vol, veh/h | 69 | 35 | 354 | 90 | 108 | 789 |
| Future Vol, veh/h | 69 | 35 | 354 | 90 | 108 | 789 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 2 | 2 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 40 | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 69 | 73 | 92 | 80 | 68 | 89 |
| Heavy Vehicles, % | 2 | 2 | 6 | 2 | 2 | 3 |
| Mvmt Flow | 100 | 48 | 385 | 113 | 159 | 887 |
| Major/Minor | Minor1 | Major1 | | Major2 | | |
| Conflicting Flow All | 1647 | 443 | 0 | 0 | 499 | 0 |
| Stage 1 | 443 | - | - | - | - | - |
| Stage 2 | 1204 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 109 | 615 | - | - | 1065 | - |
| Stage 1 | 647 | - | - | - | - | - |
| Stage 2 | 284 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | ~ 93 | 614 | - | - | 1063 | - |
| Mov Cap-2 Maneuver | ~ 93 | - | - | - | - | - |
| Stage 1 | 646 | - | - | - | - | - |
| Stage 2 | 242 | - | - | - | - | - |
| Approach | WB | NB | | SB | | |
| HCM Control Delay, s/veh | 94.76 | 0 | | 1.36 | | |
| HCM LOS | F | | | | | |
| Minor Lane/Major Mvmt | NBT | NBR | WBLn1 | SBL | SBT | |
| Capacity (veh/h) | - | - | 128 | 1063 | - | |
| HCM Lane V/C Ratio | - | - | 1.157 | 0.149 | - | |
| HCM Control Delay (s/veh) | - | - | 194.8 | 9 | - | |
| HCM Lane LOS | - | - | F | A | - | |
| HCM 95th %tile Q(veh) | - | - | 8.8 | 0.5 | - | |
| Notes | | | | | | |
| ~: Volume exceeds capacity | | \$: Delay exceeds 300s | | +: Computation Not Defined | | *: All major volume in platoon |

Lanes, Volumes, Timings

1: Beaver Bank Road & Millwood Drive/Stokil Drive

Existing PM (2024)

10/09/2024

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|-----|-------|-------|-----|-------|--------|-----|-------|-------|-----|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 101 | 44 | 110 | 84 | 68 | 81 | 129 | 830 | 81 | 19 | 426 | 83 |
| Future Volume (vph) | 101 | 44 | 110 | 84 | 68 | 81 | 129 | 830 | 81 | 19 | 426 | 83 |
| Satd. Flow (prot) | 1738 | 1627 | 0 | 1706 | 1688 | 0 | 1755 | 1831 | 0 | 1789 | 1794 | 0 |
| Flt Permitted | 0.352 | | | 0.504 | | | 0.302 | | | 0.077 | | |
| Satd. Flow (perm) | 643 | 1627 | 0 | 903 | 1688 | 0 | 558 | 1831 | 0 | 145 | 1794 | 0 |
| Satd. Flow (RTOR) | | 89 | | | 52 | | | 7 | | | 12 | |
| Lane Group Flow (vph) | 160 | 188 | 0 | 88 | 192 | 0 | 177 | 983 | 0 | 28 | 562 | 0 |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 3 | 8 | | 7 | 4 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 8 | | | 4 | | | 6 | | | 2 | | |
| Total Split (s) | 12.0 | 31.2 | | 12.0 | 31.2 | | 16.0 | 71.4 | | 12.0 | 71.4 | |
| Total Lost Time (s) | 4.0 | 6.2 | | 4.0 | 6.2 | | 4.0 | 6.4 | | 4.0 | 6.4 | |
| Act Effct Green (s) | 25.1 | 16.6 | | 23.7 | 13.8 | | 73.7 | 65.6 | | 68.0 | 58.5 | |
| Actuated g/C Ratio | 0.23 | 0.15 | | 0.21 | 0.13 | | 0.67 | 0.59 | | 0.62 | 0.53 | |
| v/c Ratio | 0.71 | 0.59 | | 0.35 | 0.75 | | 0.38 | 0.90 | | 0.14 | 0.59 | |
| Control Delay (s/veh) | 53.7 | 32.2 | | 37.2 | 52.4 | | 9.6 | 34.5 | | 9.1 | 21.5 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay (s/veh) | 53.7 | 32.2 | | 37.2 | 52.4 | | 9.6 | 34.5 | | 9.1 | 21.5 | |
| LOS | D | C | | D | D | | A | C | | A | C | |
| Approach Delay (s/veh) | | 42.1 | | | 47.6 | | | 30.7 | | | 20.9 | |
| Approach LOS | | D | | | D | | | C | | | C | |
| Queue Length 50th (m) | 29.9 | 21.1 | | 15.8 | 30.8 | | 12.6 | 194.4 | | 1.8 | 77.3 | |
| Queue Length 95th (m) | 32.4 | 40.4 | | 29.0 | 54.9 | | 19.7 | #324.2 | | 4.2 | 132.7 | |
| Internal Link Dist (m) | | 142.5 | | | 100.7 | | | 85.0 | | | 195.0 | |
| Turn Bay Length (m) | 90.0 | | | 50.0 | | | 90.0 | | | 60.0 | | |
| Base Capacity (vph) | 226 | 440 | | 255 | 425 | | 506 | 1158 | | 211 | 1070 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.71 | 0.43 | | 0.35 | 0.45 | | 0.35 | 0.85 | | 0.13 | 0.53 | |

Intersection Summary

Cycle Length: 130.6

Actuated Cycle Length: 110.3

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.90

Intersection Signal Delay (s/veh): 31.9

Intersection LOS: C

Intersection Capacity Utilization 86.9%

ICU Level of Service E

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Beaver Bank Road & Millwood Drive/Stokil Drive



| Intersection | | | | | | |
|----------------------------|-----------|------------------------|--------|----------------------------|-------|--------------------------------|
| Int Delay, s/veh | 57.2 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Y | | Y | Y | Y | Y |
| Traffic Vol, veh/h | 107 | 82 | 840 | 165 | 49 | 541 |
| Future Vol, veh/h | 107 | 82 | 840 | 165 | 49 | 541 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 3 | 3 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 40 | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 84 | 82 | 93 | 86 | 77 | 82 |
| Heavy Vehicles, % | 2 | 2 | 3 | 2 | 2 | 3 |
| Mvmt Flow | 127 | 100 | 903 | 192 | 64 | 660 |
| Major/Minor | Minor1 | Major1 | Major2 | | | |
| Conflicting Flow All | 1789 | 1002 | 0 | 0 | 1098 | 0 |
| Stage 1 | 1002 | - | - | - | - | - |
| Stage 2 | 787 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | ~ 89 | 294 | - | - | 636 | - |
| Stage 1 | 355 | - | - | - | - | - |
| Stage 2 | 448 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | ~ 80 | 293 | - | - | 634 | - |
| Mov Cap-2 Maneuver | ~ 80 | - | - | - | - | - |
| Stage 1 | 354 | - | - | - | - | - |
| Stage 2 | 403 | - | - | - | - | - |
| Approach | WB | NB | SB | | | |
| HCM Control Delay | \$ 511.64 | 0 | 0.99 | | | |
| HCM LOS | F | | | | | |
| Minor Lane/Major Mvmt | NBT | NBR | WBL | Ln1 | SBL | SBT |
| Capacity (veh/h) | - | - | 118 | 634 | - | - |
| HCM Lane V/C Ratio | - | - | 1.934 | 0.1 | - | - |
| HCM Control Delay (s/veh) | - | \$ 511.6 | 11.3 | - | - | - |
| HCM Lane LOS | - | - | F | B | - | - |
| HCM 95th %tile Q(veh) | - | - | 18.4 | 0.3 | - | - |
| Notes | | | | | | |
| ~: Volume exceeds capacity | | \$: Delay exceeds 300s | | +: Computation Not Defined | | *: All major volume in platoon |

APPENDIX C: FUTURE BACKGROUND SYNCHRO REPORTS

Lanes, Volumes, Timings

1: Beaver Bank Road & Millwood Drive/Stokil Drive

Background AM (2034)

10/09/2024

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|-----|-------|-------|-----|-------|-------|-----|-------|--------|-----|
| Lane Configurations | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | |
| Traffic Volume (vph) | 71 | 48 | 172 | 162 | 39 | 30 | 48 | 315 | 120 | 42 | 736 | 71 |
| Future Volume (vph) | 71 | 48 | 172 | 162 | 39 | 30 | 48 | 315 | 120 | 42 | 736 | 71 |
| Satd. Flow (prot) | 1789 | 1625 | 0 | 1789 | 1697 | 0 | 1789 | 1705 | 0 | 1772 | 1829 | 0 |
| Flt Permitted | 0.700 | | | 0.214 | | | 0.070 | | | 0.400 | | |
| Satd. Flow (perm) | 1315 | 1625 | 0 | 402 | 1697 | 0 | 132 | 1705 | 0 | 745 | 1829 | 0 |
| Satd. Flow (RTOR) | | 113 | | | 34 | | | 22 | | | 7 | |
| Lane Group Flow (vph) | 89 | 267 | 0 | 186 | 88 | 0 | 58 | 479 | 0 | 62 | 952 | 0 |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 3 | 8 | | 7 | 4 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 8 | | | 4 | | | 6 | | | 2 | | |
| Total Split (s) | 12.0 | 31.2 | | 12.0 | 31.2 | | 16.0 | 71.4 | | 12.0 | 71.4 | |
| Total Lost Time (s) | 4.0 | 6.2 | | 4.0 | 6.2 | | 4.0 | 6.4 | | 4.0 | 6.4 | |
| Act Effct Green (s) | 25.7 | 15.8 | | 27.1 | 18.7 | | 73.7 | 65.6 | | 73.6 | 65.6 | |
| Actuated g/C Ratio | 0.22 | 0.14 | | 0.24 | 0.16 | | 0.64 | 0.57 | | 0.64 | 0.57 | |
| v/c Ratio | 0.27 | 0.83 | | 0.97 | 0.29 | | 0.31 | 0.49 | | 0.11 | 0.91 | |
| Control Delay (s/veh) | 35.4 | 49.6 | | 97.4 | 31.1 | | 12.1 | 17.8 | | 8.3 | 38.0 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay (s/veh) | 35.4 | 49.6 | | 97.4 | 31.1 | | 12.1 | 17.8 | | 8.3 | 38.0 | |
| LOS | D | D | | F | C | | B | B | | A | D | |
| Approach Delay (s/veh) | | 46.1 | | | 76.1 | | | 17.2 | | | 36.2 | |
| Approach LOS | | D | | | E | | | B | | | D | |
| Queue Length 50th (m) | 15.9 | 35.1 | | ~35.3 | 11.2 | | 4.1 | 61.0 | | 4.4 | 190.1 | |
| Queue Length 95th (m) | 25.8 | 49.4 | | #63.0 | 25.3 | | 9.6 | 105.3 | | 8.2 | #308.3 | |
| Internal Link Dist (m) | | 142.5 | | | 100.7 | | | 85.0 | | | 195.0 | |
| Turn Bay Length (m) | 90.0 | | | 50.0 | | | 90.0 | | | 60.0 | | |
| Base Capacity (vph) | 331 | 444 | | 192 | 399 | | 262 | 1041 | | 553 | 1046 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.27 | 0.60 | | 0.97 | 0.22 | | 0.22 | 0.46 | | 0.11 | 0.91 | |

Intersection Summary

Cycle Length: 130.6

Actuated Cycle Length: 114.9

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.97

Intersection Signal Delay (s/veh): 38.1

Intersection LOS: D

Intersection Capacity Utilization 79.2%

ICU Level of Service D

Analysis Period (min) 15

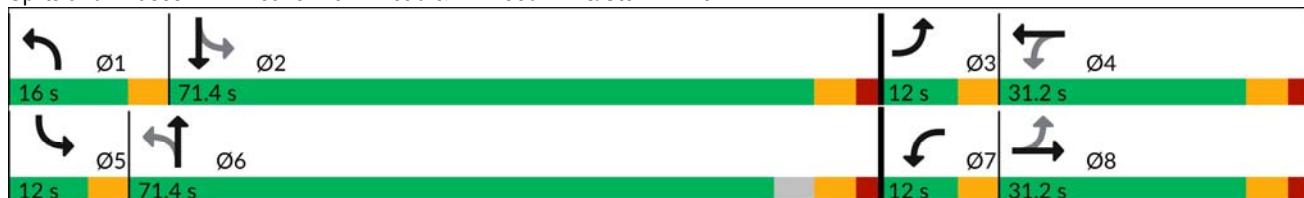
~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Beaver Bank Road & Millwood Drive/Stokil Drive



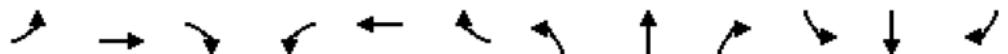
| Intersection | | | | | | |
|----------------------------|----------|------------------------|----------------------------|-------|--------------------------------|------|
| Int Delay, s/veh | 38.2 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Y | | Y | | Y | Y |
| Traffic Vol, veh/h | 77 | 39 | 392 | 100 | 120 | 872 |
| Future Vol, veh/h | 77 | 39 | 392 | 100 | 120 | 872 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 2 | 2 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 40 | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 69 | 73 | 92 | 80 | 68 | 89 |
| Heavy Vehicles, % | 2 | 2 | 6 | 2 | 2 | 3 |
| Mvmt Flow | 112 | 53 | 426 | 125 | 176 | 980 |
| Major/Minor | Minor1 | Major1 | Major2 | | | |
| Conflicting Flow All | 1823 | 491 | 0 | 0 | 553 | 0 |
| Stage 1 | 491 | - | - | - | - | - |
| Stage 2 | 1333 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | ~ 85 | 578 | - | - | 1017 | - |
| Stage 1 | 615 | - | - | - | - | - |
| Stage 2 | 246 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | ~ 70 | 577 | - | - | 1015 | - |
| Mov Cap-2 Maneuver | ~ 70 | - | - | - | - | - |
| Stage 1 | 614 | - | - | - | - | - |
| Stage 2 | 203 | - | - | - | - | - |
| Approach | WB | NB | SB | | | |
| HCM Control Delay | \$423.91 | 0 | 1.42 | | | |
| HCM LOS | F | | | | | |
| Minor Lane/Major Mvmt | NBT | NBR | WBL | Ln1 | SBL | SBT |
| Capacity (veh/h) | - | - | 98 | 1015 | - | - |
| HCM Lane V/C Ratio | - | - | 1.687 | 0.174 | - | - |
| HCM Control Delay (s/veh) | - | \$ 423.9 | 9.3 | - | - | - |
| HCM Lane LOS | - | - | F | A | - | - |
| HCM 95th %tile Q(veh) | - | - | 13.1 | 0.6 | - | - |
| Notes | | | | | | |
| ~: Volume exceeds capacity | | \$: Delay exceeds 300s | +: Computation Not Defined | | *: All major volume in platoon | |

Lanes, Volumes, Timings

1: Beaver Bank Road & Millwood Drive/Stokil Drive

Background PM (2034)

10/09/2024



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|-----|-------|-------|-----|-------|--------|-----|-------|-------|-----|
| Lane Configurations | ↑ ↘ | ↑ ↗ | | ↑ ↘ | ↑ ↗ | | ↑ ↘ | ↑ ↗ | | ↑ ↘ | ↑ ↗ | |
| Traffic Volume (vph) | 112 | 49 | 122 | 93 | 76 | 90 | 143 | 917 | 90 | 21 | 471 | 92 |
| Future Volume (vph) | 112 | 49 | 122 | 93 | 76 | 90 | 143 | 917 | 90 | 21 | 471 | 92 |
| Satd. Flow (prot) | 1738 | 1629 | 0 | 1706 | 1688 | 0 | 1755 | 1831 | 0 | 1789 | 1794 | 0 |
| Flt Permitted | 0.332 | | | 0.365 | | | 0.257 | | | 0.066 | | |
| Satd. Flow (perm) | 606 | 1629 | 0 | 654 | 1688 | 0 | 475 | 1831 | 0 | 124 | 1794 | 0 |
| Satd. Flow (RTOR) | | 89 | | | 52 | | | 7 | | | 12 | |
| Lane Group Flow (vph) | 178 | 209 | 0 | 97 | 213 | 0 | 196 | 1087 | 0 | 31 | 621 | 0 |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 3 | 8 | | 7 | 4 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 8 | | | 4 | | | 6 | | | 2 | | |
| Total Split (s) | 12.0 | 31.2 | | 12.0 | 31.2 | | 16.0 | 71.4 | | 12.0 | 71.4 | |
| Total Lost Time (s) | 4.0 | 6.2 | | 4.0 | 6.2 | | 4.0 | 6.4 | | 4.0 | 6.4 | |
| Act Effct Green (s) | 25.9 | 15.6 | | 25.3 | 15.3 | | 74.2 | 65.9 | | 67.8 | 58.4 | |
| Actuated g/C Ratio | 0.23 | 0.14 | | 0.23 | 0.14 | | 0.66 | 0.59 | | 0.60 | 0.52 | |
| v/c Ratio | 0.81 | 0.69 | | 0.44 | 0.77 | | 0.46 | 1.01 | | 0.17 | 0.66 | |
| Control Delay (s/veh) | 63.6 | 38.6 | | 39.6 | 54.5 | | 11.5 | 55.1 | | 10.2 | 24.7 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay (s/veh) | 63.6 | 38.6 | | 39.6 | 54.5 | | 11.5 | 55.1 | | 10.2 | 24.7 | |
| LOS | E | D | | D | D | | B | E | | B | C | |
| Approach Delay (s/veh) | | 50.1 | | | 49.9 | | | 48.5 | | | 24.0 | |
| Approach LOS | | D | | | D | | | D | | | C | |
| Queue Length 50th (m) | 33.7 | 26.2 | | 17.5 | 36.0 | | 14.9 | ~271.9 | | 2.1 | 94.4 | |
| Queue Length 95th (m) | 36.0 | 47.0 | | 31.8 | 62.4 | | 22.9 | #390.9 | | 4.7 | 159.2 | |
| Internal Link Dist (m) | | 142.5 | | | 100.7 | | | 85.0 | | | 195.0 | |
| Turn Bay Length (m) | 90.0 | | | 50.0 | | | 90.0 | | | 60.0 | | |
| Base Capacity (vph) | 221 | 435 | | 225 | 420 | | 453 | 1139 | | 196 | 1054 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.81 | 0.48 | | 0.43 | 0.51 | | 0.43 | 0.95 | | 0.16 | 0.59 | |

Intersection Summary

Cycle Length: 130.6

Actuated Cycle Length: 112.2

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 1.01

Intersection Signal Delay (s/veh): 42.8

Intersection LOS: D

Intersection Capacity Utilization 93.0%

ICU Level of Service F

Analysis Period (min) 15

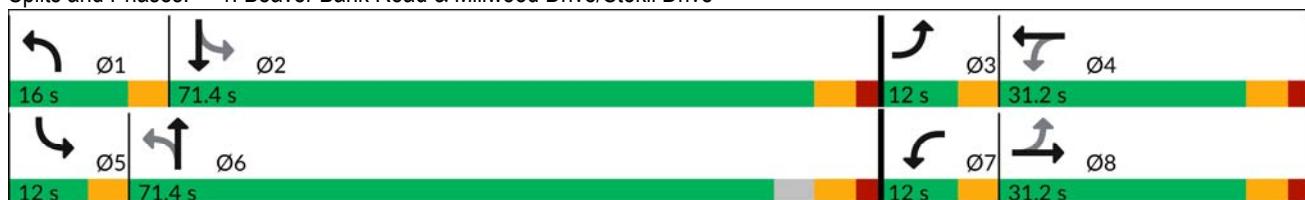
~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Beaver Bank Road & Millwood Drive/Stokil Drive



| Intersection | | | | | | |
|----------------------------|----------|------------------------|--------|----------------------------|-------|--------------------------------|
| Int Delay, s/veh | 103.7 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Y | | Y | | Y | Y |
| Traffic Vol, veh/h | 119 | 91 | 928 | 183 | 55 | 598 |
| Future Vol, veh/h | 119 | 91 | 928 | 183 | 55 | 598 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 3 | 3 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 40 | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 84 | 82 | 93 | 86 | 77 | 82 |
| Heavy Vehicles, % | 2 | 2 | 3 | 2 | 2 | 3 |
| Mvmt Flow | 142 | 111 | 998 | 213 | 71 | 729 |
| Major/Minor | Minor1 | Major1 | Major2 | | | |
| Conflicting Flow All | 1979 | 1107 | 0 | 0 | 1214 | 0 |
| Stage 1 | 1107 | - | - | - | - | - |
| Stage 2 | 872 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | ~ 68 | 256 | - | - | 575 | - |
| Stage 1 | 316 | - | - | - | - | - |
| Stage 2 | 409 | - | - | - | - | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | ~ 59 | 255 | - | - | 573 | - |
| Mov Cap-2 Maneuver | ~ 59 | - | - | - | - | - |
| Stage 1 | 315 | - | - | - | - | - |
| Stage 2 | 358 | - | - | - | - | - |
| Approach | WB | NB | SB | | | |
| HCM Control Delay | \$926.05 | 0 | 1.09 | | | |
| HCM LOS | F | | | | | |
| Minor Lane/Major Mvmt | NBT | NBR | WBL | Ln1 | SBL | SBT |
| Capacity (veh/h) | - | - | 89 | 573 | - | - |
| HCM Lane V/C Ratio | - | - | 2.828 | 0.125 | - | - |
| HCM Control Delay (s/veh) | - | - | \$ 926 | 12.2 | - | - |
| HCM Lane LOS | - | - | F | B | - | - |
| HCM 95th %tile Q(veh) | - | - | 24.3 | 0.4 | - | - |
| Notes | | | | | | |
| ~: Volume exceeds capacity | | \$: Delay exceeds 300s | | +: Computation Not Defined | | *: All major volume in platoon |

APPENDIX D: TRAFFIC SIGNAL WARRANT ANALYSIS



HRM - Traffic Signal & Pedestrian Signal Head Warrant Analysis

| | |
|--------------------------------|-----------------|
| Main Street (name) | Beaverbank Road |
| Side Street (name) | Windgate Drive |
| Quadrant / Int # | |
| Comments CHECK SHEET | |

for Warrant Calculation Results, please hit 'Page Down'

| | |
|---------------------------------|----|
| Direction (EW or NS) | NS |
| Direction (EW or NS) | EW |
| Existing Traffic Volumes | |

| | |
|--------------------|------------------|
| Road Authority: | HRM |
| City: | HRM |
| Analysis Date: | 2024 Oct 04, Fri |
| Count Date: | 2023 Jun 22, Thu |
| Date Entry Format: | (yyyy-mm-dd) |

| Lane Configuration | | Excl LT | Th & LT | Through | Th+RT+LT | Th & RT | Excl RT | RT Channelization(y/n) | UpStream Signal(m) | # of Thru Lanes | LT Phase Type | RTOR Allowed(y/n) | Actuated Thru Phase | Saturation Flow Rates (if not default) (vphpl) | Default Saturation Flow Rates (vphpl) |
|--------------------|----|---------|---------|---------|----------|---------|---------|------------------------|--------------------|-----------------|---------------|-------------------|---------------------|--|---------------------------------------|
| Beaverbank Road | NB | | | | | 1 | | | 1,700 | 1 | | | | Left Turn | 1,650 |
| Beaverbank Road | SB | 1 | | 1 | | | | | 590 | 1 | | | | Through | 1,800 |
| Windgate Drive | WB | | | | 1 | | | | 1,700 | 1 | | | | Right Turn | 1,500 |
| Windgate Drive | EB | | | | | | | | 0 | | | | | | |

Are the Windgate Drive WB right turns significantly impeded by through movements? (y/n) **y**

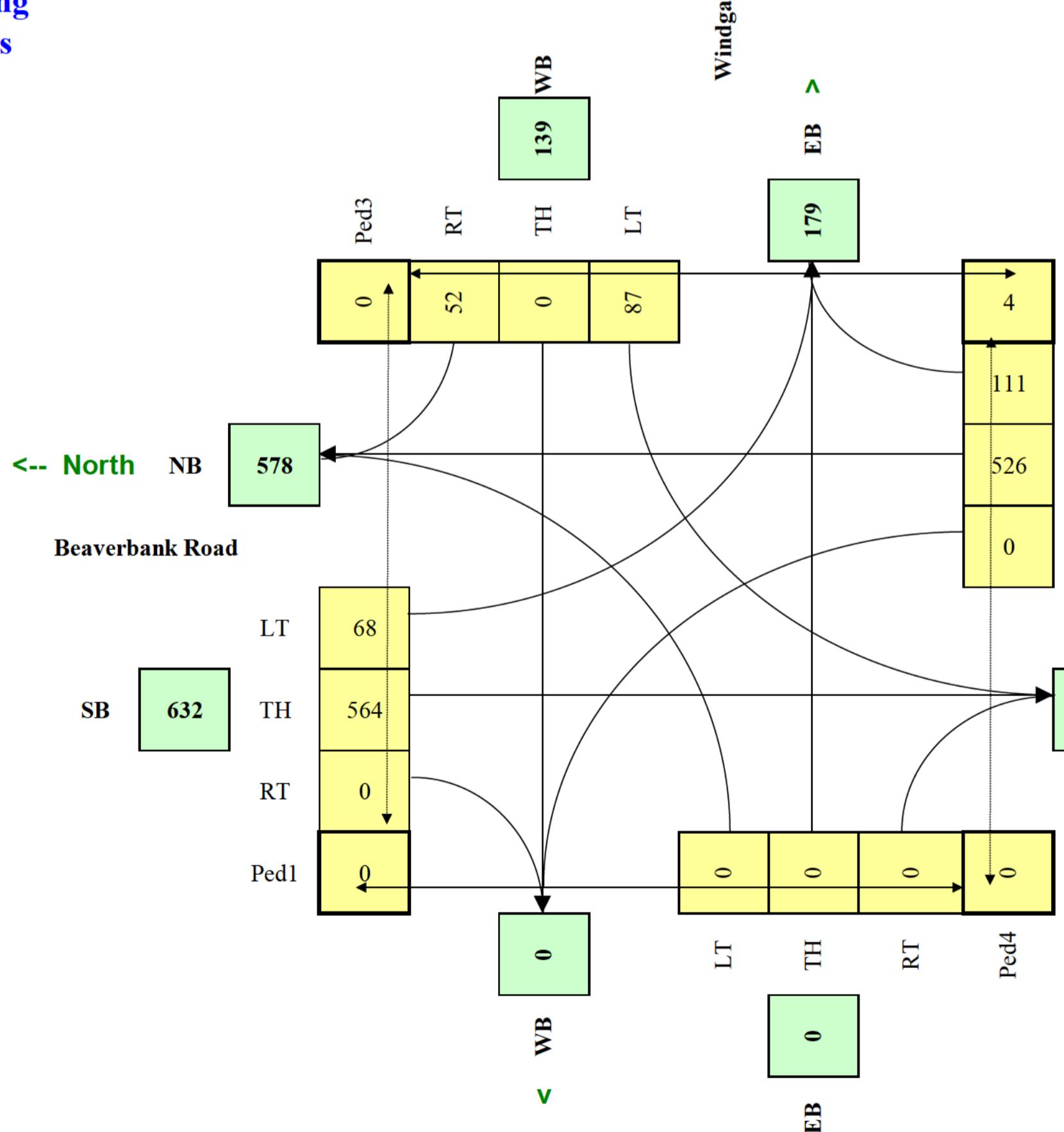
Are the Beaverbank Road NB right turns significantly impeded by through movements? (y/n) **y**

| Other input | | Speed (Km/h) | Truck % | Bus Rt (y/n) | Median (m) |
|-----------------|----|--------------|---------|--------------|------------|
| Beaverbank Road | NS | 50 | 4.0% | y | |
| Windgate Drive | EW | 70 | 3.0% | n | |

| Demographics | |
|----------------------------------|---------|
| Elem. School/Mobility Challenged | (y/n) |
| Senior's Complex | (y/n) |
| Pathway to School | (y/n) |
| Metro Area Population (#) | 465,703 |
| Central Business District | (y/n) |

| Set Peak Hours | | | Actual Pedestrian Crossing Distance (m) | | | | | | | | | | | | | |
|-----------------------|-----|-------|---|-----|-------|----|-----|----|-----|----|----|----|--------|--------|--------|--------|
| Traffic Input | NB | | | SB | | | WB | | | EB | | | NS | NS | EW | EW |
| | LT | Th | RT | LT | Th | RT | LT | Th | RT | LT | Th | RT | W Side | E Side | N Side | S Side |
| 0: - 0: | 329 | 86 | 106 | 818 | | | 65 | | 40 | | | | | 5 | | |
| | 311 | 88 | 84 | 660 | | | 73 | | 21 | | | | | 3 | | |
| | 399 | 91 | 58 | 429 | | | 89 | | 50 | | | | | 3 | | |
| | 464 | 100 | 55 | 425 | | | 84 | | 43 | | | | | 3 | | |
| | 843 | 139 | 47 | 500 | | | 102 | | 79 | | | | | 5 | | |
| | 811 | 162 | 55 | 554 | | | 110 | | 80 | | | | | 5 | | |
| Total (6-hour peak) | 0 | 3,157 | 666 | 405 | 3,386 | 0 | 523 | 0 | 313 | 0 | 0 | 0 | 0 | 24 | 0 | 0 |
| Average (6-hour peak) | 0 | 526 | 111 | 68 | 564 | 0 | 87 | 0 | 52 | 0 | 0 | 0 | 0 | 4 | 0 | 0 |

Average 6-hour Peak Turning Movements



$$W_{SIG} = [C_{bt}(X_{v-v}) / K_1 + (F(X_{v-p})L) / K_2] \times C_i$$

$$W = \begin{matrix} 91 & 91 & 0 \\ Veh & Ped \end{matrix}$$

NOT Warranted

RESET SHEET

RT TH 637 NB

LT

Beaverbank Road

SB >

$$W_{PED} = [F((X_{ped_m})d_m/K_2) + (X_{ped_s})d_s/K_3)]$$

$$W = \begin{matrix} 0 \end{matrix}$$

Warranted - Complex Intersection



HRM - Traffic Signal & Pedestrian Signal Head Warrant Analysis

| | |
|---|-----------------|
| Main Street (name) | Beaverbank Road |
| Side Street (name) | Windgate Drive |
| Quadrant / Int # | |
| for Warrant Calculation Results, please hit 'Page Down' | CHECK SHEET |

| | |
|----------|--|
| Comments | Direction (EW or NS) NS |
| | Direction (EW or NS) EW |
| | Future Background (2034) Traffic Volumes |

| | |
|--------------------|------------------|
| Road Authority: | HRM |
| City: | HRM |
| Analysis Date: | 2024 Oct 08, Tue |
| Count Date: | 2023 Jun 22, Thu |
| Date Entry Format: | (yyyy-mm-dd) |

| Lane Configuration | | Excl LT | Th & LT | Through | Th+RT+LT | Th & RT | Excl RT | RT Channelization(y/n) | UpStream Signal(m) | # of Thru Lanes | LT Phase Type | RTOR Allowed(y/n) | Actuated Thru Phase | Saturation Flow Rates (if not default) (vphpl) | Default Saturation Flow Rates (vphpl) |
|--------------------|----|---------|---------|---------|----------|---------|---------|------------------------|--------------------|-----------------|---------------|-------------------|---------------------|--|---------------------------------------|
| Beaverbank Road | NB | | | | | 1 | | | 1,700 | 1 | | | | Left Turn | 1,650 |
| Beaverbank Road | SB | 1 | | 1 | | | | | 590 | 1 | | | | Through | 1,800 |
| Windgate Drive | WB | | | | 1 | | | | 1,700 | 1 | | | | Right Turn | 1,500 |
| Windgate Drive | EB | | | | | | | | 0 | | | | | | |

Are the Windgate Drive WB right turns significantly impeded by through movements? (y/n) y

Are the Beaverbank Road NB right turns significantly impeded by through movements? (y/n) y

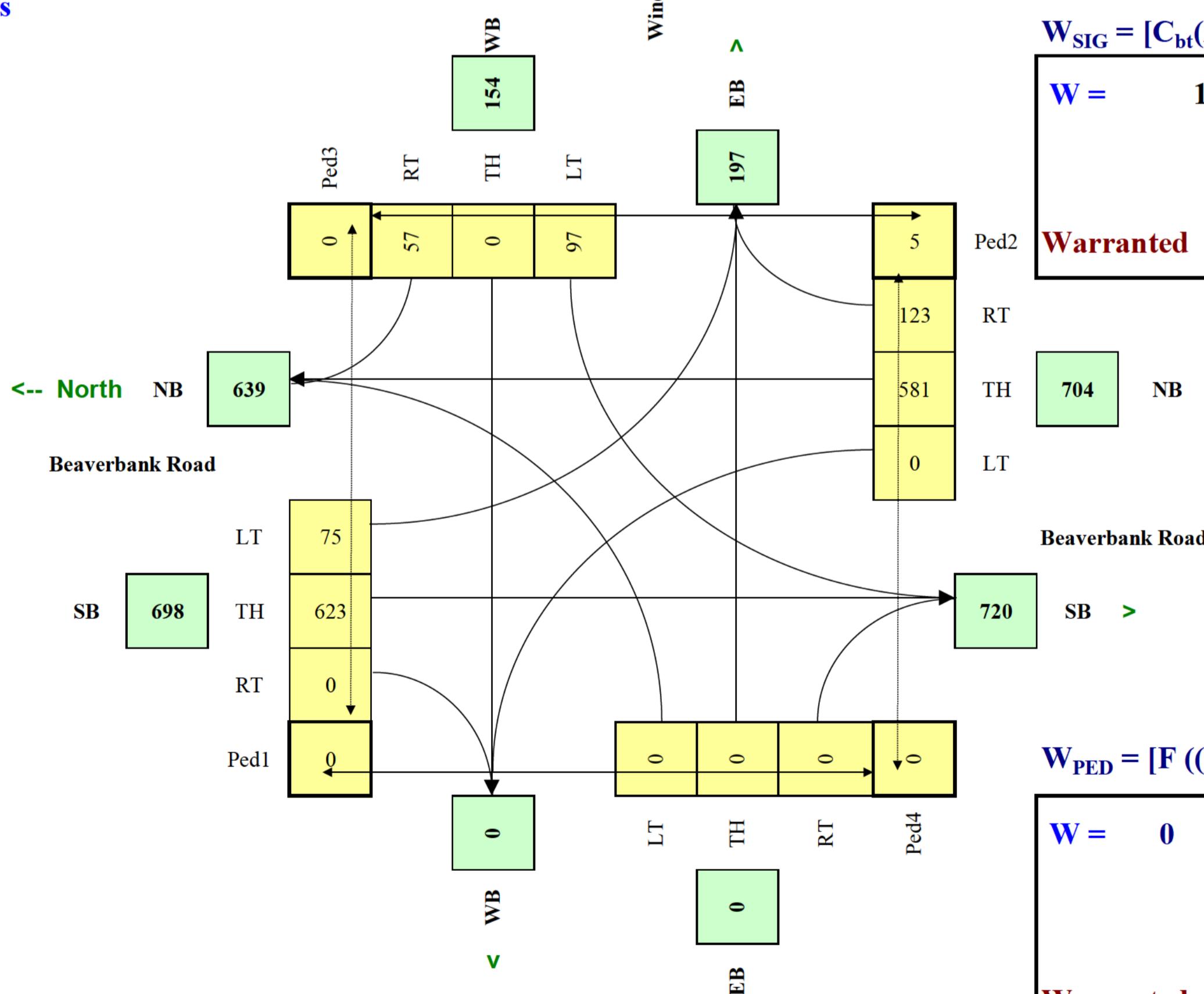
| Other input | | Speed (Km/h) | Truck % | Bus Rt (y/n) | Median (m) |
|-----------------|----|--------------|---------|--------------|------------|
| Beaverbank Road | NS | 50 | 4.0% | y | |
| Windgate Drive | EW | 70 | 3.0% | n | |

| Demographics | |
|----------------------------------|---------|
| Elem. School/Mobility Challenged | (y/n) |
| Senior's Complex | (y/n) |
| Pathway to School | (y/n) |
| Metro Area Population (#) | 465,703 |
| Central Business District | (y/n) |

| Set Peak Hours | | | | | | | | | | | | | Ped1 | Ped2 | Ped3 | Ped4 |
|-----------------------|-----|-------|-----|-----|-------|----|-----|----|-----|----|----|----|--------|--------|--------|--------|
| | NB | | | SB | | | WB | | | EB | | | NS | NS | EW | EW |
| Traffic Input | LT | Th | RT | LT | Th | RT | LT | Th | RT | LT | Th | RT | W Side | E Side | N Side | S Side |
| 0: - 0: | 363 | 95 | 117 | 904 | | | 72 | | 44 | | | | | | 6 | |
| | 344 | 97 | 93 | 729 | | | 81 | | 23 | | | | | | 3 | |
| | 441 | 101 | 64 | 474 | | | 98 | | 55 | | | | | | 3 | |
| | 513 | 110 | 61 | 469 | | | 93 | | 47 | | | | | | 3 | |
| | 931 | 154 | 52 | 552 | | | 113 | | 87 | | | | | | 6 | |
| | 896 | 179 | 61 | 612 | | | 122 | | 88 | | | | | | 6 | |
| Total (6-hour peak) | 0 | 3,488 | 736 | 448 | 3,740 | 0 | 579 | 0 | 344 | 0 | 0 | 0 | 0 | 27 | 0 | 0 |
| Average (6-hour peak) | 0 | 581 | 123 | 75 | 623 | 0 | 97 | 0 | 57 | 0 | 0 | 0 | 0 | 5 | 0 | 0 |

Actual Pedestrian Crossing Distance (m)

Average 6-hour Peak Turning Movements



$$W_{SIG} = [C_{bt}(X_{v-v}) / K_1 + (F(X_{v-p})L) / K_2] \times C_i$$

$$W = \begin{matrix} 111 & 111 & 0 \\ Veh & Ped \end{matrix}$$

Warranted

RESET SHEET

RT

TH

NB

LT

Beaverbank Road

SB

>

$$W_{PED} = [F((X_{ped_m})d_m/K_2) + (X_{ped_s})d_s/K_3)]$$

$$W = 0$$

Warranted - Complex Intersection

APPENDIX E: FUTURE BACKGROUND MITIGATION SYNCHRO REPORTS

Lanes, Volumes, Timings

1: Beaver Bank Road & Millwood Drive/Stokil Drive

Background AM (2034)-Mitigation

10/09/2024

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|-----|-------|-------|-----|-------|------|-----|-------|--------|-----|
| Lane Configurations | ↑ | ↓ | | ↑ | ↓ | | ↑ | ↓ | | ↑ | ↓ | |
| Traffic Volume (vph) | 71 | 48 | 172 | 162 | 39 | 30 | 48 | 315 | 120 | 42 | 736 | 71 |
| Future Volume (vph) | 71 | 48 | 172 | 162 | 39 | 30 | 48 | 315 | 120 | 42 | 736 | 71 |
| Satd. Flow (prot) | 1789 | 1625 | 0 | 1789 | 1697 | 0 | 1789 | 1705 | 0 | 1772 | 1829 | 0 |
| Flt Permitted | 0.700 | | | 0.188 | | | 0.062 | | | 0.391 | | |
| Satd. Flow (perm) | 1315 | 1625 | 0 | 354 | 1697 | 0 | 117 | 1705 | 0 | 729 | 1829 | 0 |
| Satd. Flow (RTOR) | | 109 | | | 34 | | | 23 | | | 8 | |
| Lane Group Flow (vph) | 89 | 267 | 0 | 186 | 88 | 0 | 58 | 479 | 0 | 62 | 952 | 0 |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 3 | 8 | | 7 | 4 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 8 | | | 4 | | | 6 | | | 2 | | |
| Total Split (s) | 11.0 | 27.5 | | 14.0 | 30.5 | | 11.0 | 78.1 | | 11.0 | 78.1 | |
| Total Lost Time (s) | 4.0 | 6.2 | | 4.0 | 6.2 | | 4.0 | 6.4 | | 4.0 | 6.4 | |
| Act Effct Green (s) | 25.6 | 16.0 | | 32.2 | 22.5 | | 72.5 | 64.8 | | 72.5 | 64.8 | |
| Actuated g/C Ratio | 0.22 | 0.14 | | 0.28 | 0.19 | | 0.62 | 0.56 | | 0.62 | 0.56 | |
| v/c Ratio | 0.28 | 0.84 | | 0.83 | 0.25 | | 0.33 | 0.50 | | 0.12 | 0.93 | |
| Control Delay (s/veh) | 38.2 | 53.5 | | 66.9 | 32.0 | | 13.2 | 18.1 | | 8.4 | 41.8 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay (s/veh) | 38.2 | 53.5 | | 66.9 | 32.0 | | 13.2 | 18.1 | | 8.4 | 41.8 | |
| LOS | D | D | | E | C | | B | B | | A | D | |
| Approach Delay (s/veh) | | 49.7 | | | 55.7 | | | 17.6 | | | 39.7 | |
| Approach LOS | | D | | | E | | | B | | | D | |
| Queue Length 50th (m) | 17.2 | 39.6 | | 38.2 | 11.8 | | 4.6 | 66.0 | | 4.9 | 206.2 | |
| Queue Length 95th (m) | 27.1 | 53.7 | | #65.6 | 26.2 | | 9.1 | 99.4 | | 7.7 | #296.8 | |
| Internal Link Dist (m) | | 142.5 | | | 100.7 | | | 85.0 | | | 195.0 | |
| Turn Bay Length (m) | 90.0 | | | 50.0 | | | 90.0 | | | 60.0 | | |
| Base Capacity (vph) | 318 | 397 | | 225 | 395 | | 177 | 1100 | | 517 | 1174 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.28 | 0.67 | | 0.83 | 0.22 | | 0.33 | 0.44 | | 0.12 | 0.81 | |

Intersection Summary

Cycle Length: 130.6

Actuated Cycle Length: 116.7

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.93

Intersection Signal Delay (s/veh): 37.9

Intersection LOS: D

Intersection Capacity Utilization 79.2%

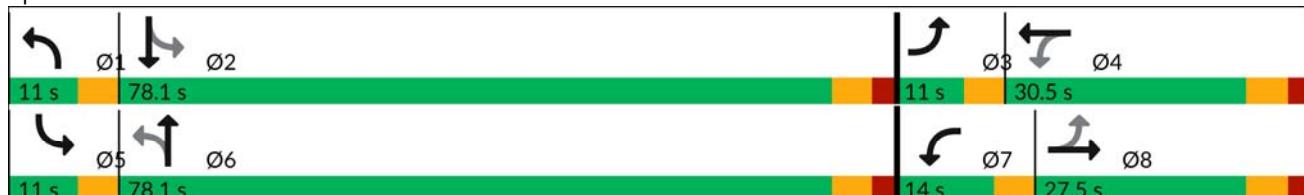
ICU Level of Service D

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Beaver Bank Road & Millwood Drive/Stokil Drive



Lanes, Volumes, Timings
2: Beaver Bank Road & Windgate Drive

Background AM (2034)-Mitigation
10/09/2024



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|------------------------|-------|-----|-------|------|-------|-------|
| Lane Configurations | WBL | WBR | NBT | NBR | SBL | SBT |
| Traffic Volume (vph) | 77 | 39 | 392 | 100 | 120 | 872 |
| Future Volume (vph) | 77 | 39 | 392 | 100 | 120 | 872 |
| Satd. Flow (prot) | 1743 | 0 | 1812 | 1601 | 1789 | 1865 |
| Flt Permitted | 0.967 | | | | 0.498 | |
| Satd. Flow (perm) | 1743 | 0 | 1812 | 1564 | 936 | 1865 |
| Satd. Flow (RTOR) | 25 | | | 125 | | |
| Lane Group Flow (vph) | 165 | 0 | 426 | 125 | 176 | 980 |
| Turn Type | Prot | | NA | Perm | Perm | NA |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | | 2 | 6 | |
| Total Split (s) | 27.0 | | 63.0 | 63.0 | 63.0 | 63.0 |
| Total Lost Time (s) | 6.0 | | 6.0 | 6.0 | 6.0 | 6.0 |
| Act Effct Green (s) | 12.1 | | 46.5 | 46.5 | 46.5 | 46.5 |
| Actuated g/C Ratio | 0.17 | | 0.65 | 0.65 | 0.65 | 0.65 |
| v/c Ratio | 0.52 | | 0.36 | 0.12 | 0.29 | 0.80 |
| Control Delay (s/veh) | 29.9 | | 7.0 | 1.5 | 7.4 | 16.3 |
| Queue Delay | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay (s/veh) | 29.9 | | 7.0 | 1.5 | 7.4 | 16.3 |
| LOS | C | | A | A | A | B |
| Approach Delay (s/veh) | 29.9 | | 5.8 | | | 14.9 |
| Approach LOS | C | | A | | | B |
| Queue Length 50th (m) | 15.9 | | 20.6 | 0.0 | 8.0 | 76.5 |
| Queue Length 95th (m) | 27.0 | | 48.3 | 4.1 | 15.8 | 175.8 |
| Internal Link Dist (m) | 279.7 | | 119.4 | | | 97.2 |
| Turn Bay Length (m) | | | 25.0 | 40.0 | | |
| Base Capacity (vph) | 548 | | 1498 | 1315 | 774 | 1542 |
| Starvation Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.30 | | 0.28 | 0.10 | 0.23 | 0.64 |

Intersection Summary

Cycle Length: 90

Actuated Cycle Length: 71

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.80

Intersection Signal Delay (s/veh): 13.5

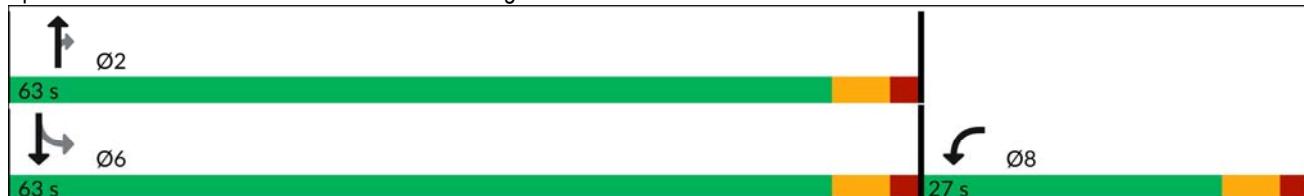
Intersection LOS: B

Intersection Capacity Utilization 62.5%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 2: Beaver Bank Road & Windgate Drive



Lanes, Volumes, Timings

1: Beaver Bank Road & Millwood Drive/Stokil Drive

Background PM (2034)-Mitigation

10/09/2024

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|-----|-------|-------|-----|-------------|------|-----|-------|-------|-----|
| Lane Configurations | ↑ | ↑ | → | ↑ | ↑ | ← | ↑ | ↑ | ↑ | ↑ | ↓ | ↑ |
| Traffic Volume (vph) | 112 | 49 | 122 | 93 | 76 | 90 | 143 | 917 | 90 | 21 | 471 | 92 |
| Future Volume (vph) | 112 | 49 | 122 | 93 | 76 | 90 | 143 | 917 | 90 | 21 | 471 | 92 |
| Satd. Flow (prot) | 1738 | 1629 | 0 | 1706 | 1688 | 0 | 1755 | 1831 | 0 | 1789 | 1794 | 0 |
| Flt Permitted | 0.301 | | | 0.314 | | | 0.279 | | | 0.058 | | |
| Satd. Flow (perm) | 550 | 1629 | 0 | 563 | 1688 | 0 | 515 | 1831 | 0 | 109 | 1794 | 0 |
| Satd. Flow (RTOR) | | 86 | | | 51 | | | 7 | | | 13 | |
| Lane Group Flow (vph) | 178 | 209 | 0 | 97 | 213 | 0 | 196 | 1087 | 0 | 31 | 621 | 0 |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 3 | 8 | | 7 | 4 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 8 | | | 4 | | | 6 | | | 2 | | |
| Total Split (s) | 11.0 | 27.9 | | 11.0 | 27.9 | | 17.0 | 80.7 | | 11.0 | 74.7 | |
| Total Lost Time (s) | 4.0 | 6.2 | | 4.0 | 6.2 | | 4.0 | 6.4 | | 4.0 | 6.4 | |
| Act Effct Green (s) | 24.9 | 15.6 | | 24.9 | 15.6 | | 83.2 | 74.8 | | 76.7 | 67.2 | |
| Actuated g/C Ratio | 0.21 | 0.13 | | 0.21 | 0.13 | | 0.69 | 0.62 | | 0.64 | 0.56 | |
| v/c Ratio | 0.97 | 0.73 | | 0.53 | 0.81 | | 0.43 | 0.95 | | 0.19 | 0.62 | |
| Control Delay (s/veh) | 104.1 | 45.0 | | 49.2 | 62.3 | | 9.9 | 41.4 | | 9.7 | 21.9 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay (s/veh) | 104.1 | 45.0 | | 49.2 | 62.3 | | 9.9 | 41.4 | | 9.7 | 21.9 | |
| LOS | F | D | | E | | | A | D | | A | C | |
| Approach Delay (s/veh) | | 72.2 | | | 58.2 | | | 36.6 | | | 21.3 | |
| Approach LOS | | E | | | E | | | D | | | C | |
| Queue Length 50th (m) | 37.6 | 29.4 | | 19.5 | 39.5 | | 14.9 ~255.0 | | | 2.1 | 94.0 | |
| Queue Length 95th (m) | 39.2 | 50.8 | | 34.4 | 66.6 | | 20.8 #381.9 | | | 4.3 | 150.9 | |
| Internal Link Dist (m) | | 142.5 | | | 100.7 | | | 85.0 | | | 195.0 | |
| Turn Bay Length (m) | 90.0 | | | 50.0 | | | 90.0 | | | 60.0 | | |
| Base Capacity (vph) | 183 | 366 | | 183 | 347 | | 491 | 1140 | | 167 | 1044 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.97 | 0.57 | | 0.53 | 0.61 | | 0.40 | 0.95 | | 0.19 | 0.59 | |

Intersection Summary

Cycle Length: 130.6

Actuated Cycle Length: 120.4

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.97

Intersection Signal Delay (s/veh): 40.6

Intersection LOS: D

Intersection Capacity Utilization 93.0%

ICU Level of Service F

Analysis Period (min) 15

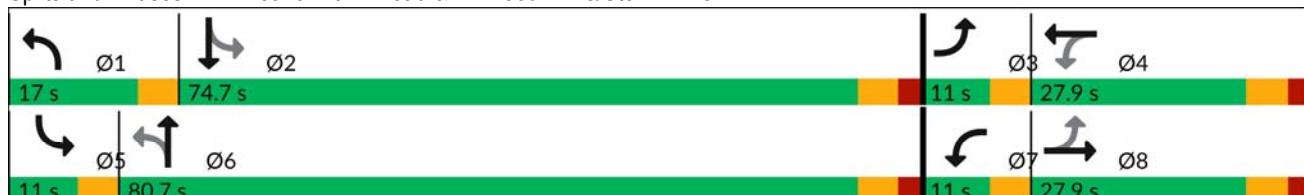
~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Beaver Bank Road & Millwood Drive/Stokil Drive



Lanes, Volumes, Timings
2: Beaver Bank Road & Windgate Drive

Background PM (2034)-Mitigation
10/09/2024



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|------------------------|-------|-----|-------|------|-------|------|
| Lane Configurations | WBL | WBR | NBT | NBR | SBL | SBT |
| Traffic Volume (vph) | 119 | 91 | 928 | 183 | 55 | 598 |
| Future Volume (vph) | 119 | 91 | 928 | 183 | 55 | 598 |
| Satd. Flow (prot) | 1724 | 0 | 1865 | 1601 | 1789 | 1865 |
| Flt Permitted | 0.973 | | | | 0.131 | |
| Satd. Flow (perm) | 1724 | 0 | 1865 | 1560 | 247 | 1865 |
| Satd. Flow (RTOR) | 36 | | | 100 | | |
| Lane Group Flow (vph) | 253 | 0 | 998 | 213 | 71 | 729 |
| Turn Type | Prot | | NA | Perm | Perm | NA |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | 2 | | 6 | |
| Total Split (s) | 27.0 | | 73.0 | 73.0 | 73.0 | 73.0 |
| Total Lost Time (s) | 6.0 | | 6.0 | 6.0 | 6.0 | 6.0 |
| Act Effct Green (s) | 15.2 | | 49.3 | 49.3 | 49.3 | 49.3 |
| Actuated g/C Ratio | 0.20 | | 0.64 | 0.64 | 0.64 | 0.64 |
| v/c Ratio | 0.69 | | 0.84 | 0.21 | 0.45 | 0.61 |
| Control Delay (s/veh) | 37.8 | | 18.9 | 3.7 | 18.5 | 11.0 |
| Queue Delay | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay (s/veh) | 37.8 | | 18.9 | 3.7 | 18.5 | 11.0 |
| LOS | D | B | A | B | B | |
| Approach Delay (s/veh) | 37.8 | | 16.2 | | | 11.7 |
| Approach LOS | D | B | | | B | |
| Queue Length 50th (m) | 29.2 | | 97.5 | 5.6 | 4.5 | 54.4 |
| Queue Length 95th (m) | 58.7 | | 183.1 | 13.6 | 13.1 | 82.8 |
| Internal Link Dist (m) | 276.3 | | 119.4 | | | 97.2 |
| Turn Bay Length (m) | | | 25.0 | 40.0 | | |
| Base Capacity (vph) | 525 | | 1578 | 1335 | 209 | 1578 |
| Starvation Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.48 | | 0.63 | 0.16 | 0.34 | 0.46 |

Intersection Summary

Cycle Length: 100

Actuated Cycle Length: 77.3

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.84

Intersection Signal Delay (s/veh): 17.0

Intersection LOS: B

Intersection Capacity Utilization 71.0%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 2: Beaver Bank Road & Windgate Drive



APPENDIX F: FUTURE TOTAL SYNCHRO REPORTS

Lanes, Volumes, Timings

Total AM (2034)

1: Beaver Bank Road & Millwood Drive/Stokil Drive

10/11/2024

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|-------|-------|------|-------|-------|-----|-------|--------|-----|
| Lane Configurations | ↑ | ↓ | | ↑ | ↓ | | ↑ | ↓ | | ↑ | ↓ | |
| Traffic Volume (vph) | 76 | 48 | 172 | 162 | 39 | 32 | 48 | 335 | 120 | 46 | 814 | 78 |
| Future Volume (vph) | 76 | 48 | 172 | 162 | 39 | 32 | 48 | 335 | 120 | 46 | 814 | 78 |
| Satd. Flow (prot) | 1789 | 1625 | 0 | 1789 | 1693 | 0 | 1789 | 1707 | 0 | 1772 | 1829 | 0 |
| Flt Permitted | 0.698 | | | | | | | 0.055 | | | 0.388 | |
| Satd. Flow (perm) | 1311 | 1625 | 0 | 387 | 1693 | 0 | 104 | 1707 | 0 | 723 | 1829 | 0 |
| Satd. Flow (RTOR) | | 109 | | | | 36 | | | 21 | | | 8 |
| Lane Group Flow (vph) | 95 | 267 | 0 | 186 | 91 | 0 | 58 | 501 | 0 | 68 | 1052 | 0 |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 3 | 8 | | 7 | 4 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 8 | | | 4 | | | 6 | | | 2 | | |
| Total Split (s) | 11.0 | 27.5 | | 14.0 | 30.5 | | 11.0 | 78.1 | | 11.0 | 78.1 | |
| Total Lost Time (s) | 4.0 | 6.2 | | 4.0 | 6.2 | | 4.0 | 6.4 | | 4.0 | 6.4 | |
| Act Effct Green (s) | 25.5 | 16.3 | | 31.5 | 19.3 | | 79.9 | 72.1 | | 79.9 | 72.1 | |
| Actuated g/C Ratio | 0.21 | 0.13 | | 0.25 | 0.16 | | 0.65 | 0.58 | | 0.65 | 0.58 | |
| v/c Ratio | 0.32 | 0.87 | | 0.88 | 0.31 | | 0.36 | 0.50 | | 0.13 | 0.98 | |
| Control Delay (s/veh) | 39.5 | 57.6 | | 76.4 | 31.9 | | 16.3 | 18.0 | | 8.4 | 51.0 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay (s/veh) | 39.5 | 57.6 | | 76.4 | 31.9 | | 16.3 | 18.0 | | 8.4 | 51.0 | |
| LOS | D | E | | E | C | | B | B | | A | D | |
| Approach Delay (s/veh) | | 52.9 | | | 61.8 | | | 17.8 | | | 48.4 | |
| Approach LOS | | D | | | E | | | B | | | D | |
| Queue Length 50th (m) | 18.5 | 39.6 | | 38.2 | 12.0 | | 4.6 | 70.8 | | 5.4 | ~277.9 | |
| Queue Length 95th (m) | 28.6 | 53.7 | | #62.0 | 26.5 | | 9.8 | 106.1 | | 8.4 | #350.6 | |
| Internal Link Dist (m) | | 142.5 | | | 100.7 | | | 85.0 | | | 195.0 | |
| Turn Bay Length (m) | 90.0 | | 50.0 | | | 90.0 | | | | 60.0 | | |
| Base Capacity (vph) | 297 | 371 | | 212 | 363 | | 163 | 1004 | | 527 | 1069 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 0.32 | 0.72 | | 0.88 | 0.25 | | 0.36 | 0.50 | | 0.13 | 0.98 | |

Intersection Summary

Cycle Length: 130.6

Actuated Cycle Length: 123.6

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.98

Intersection Signal Delay (s/veh): 43.3

Intersection LOS: D

Intersection Capacity Utilization 83.7%

ICU Level of Service E

Analysis Period (min) 15

~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Beaver Bank Road & Millwood Drive/Stokil Drive



Lanes, Volumes, Timings
2: Beaver Bank Road & Windgate Drive

Total AM (2034)

10/11/2024



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|------------------------|-------|-----|-------|------|-------|--------|
| Lane Configurations | ↔ | ↑ | ↑ | ↑ | ↔ | ↑ |
| Traffic Volume (vph) | 77 | 42 | 419 | 100 | 132 | 961 |
| Future Volume (vph) | 77 | 42 | 419 | 100 | 132 | 961 |
| Satd. Flow (prot) | 1739 | 0 | 1812 | 1601 | 1789 | 1865 |
| Flt Permitted | 0.968 | | | | 0.479 | |
| Satd. Flow (perm) | 1739 | 0 | 1812 | 1563 | 901 | 1865 |
| Satd. Flow (RTOR) | 24 | | | 125 | | |
| Lane Group Flow (vph) | 170 | 0 | 455 | 125 | 194 | 1080 |
| Turn Type | Prot | | NA | Perm | Perm | NA |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | | 2 | 6 | |
| Total Split (s) | 27.0 | | 73.0 | 73.0 | 73.0 | 73.0 |
| Total Lost Time (s) | 6.0 | | 6.0 | 6.0 | 6.0 | 6.0 |
| Act Effct Green (s) | 13.0 | | 56.2 | 56.2 | 56.2 | 56.2 |
| Actuated g/C Ratio | 0.16 | | 0.69 | 0.69 | 0.69 | 0.69 |
| v/c Ratio | 0.57 | | 0.36 | 0.11 | 0.31 | 0.84 |
| Control Delay (s/veh) | 36.6 | | 6.6 | 1.3 | 7.2 | 17.9 |
| Queue Delay | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay (s/veh) | 36.6 | | 6.6 | 1.3 | 7.2 | 17.9 |
| LOS | D | | A | A | A | B |
| Approach Delay (s/veh) | 36.6 | | 5.5 | | | 16.3 |
| Approach LOS | D | | A | | | B |
| Queue Length 50th (m) | 20.6 | | 24.4 | 0.0 | 9.9 | 103.2 |
| Queue Length 95th (m) | 31.5 | | 51.0 | 3.8 | 17.1 | #216.6 |
| Internal Link Dist (m) | 279.7 | | 119.4 | | | 97.2 |
| Turn Bay Length (m) | | | | 25.0 | 40.0 | |
| Base Capacity (vph) | 479 | | 1514 | 1326 | 752 | 1558 |
| Starvation Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.35 | | 0.30 | 0.09 | 0.26 | 0.69 |

Intersection Summary

Cycle Length: 100

Actuated Cycle Length: 81.6

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.84

Intersection Signal Delay (s/veh): 14.9

Intersection LOS: B

Intersection Capacity Utilization 67.4%

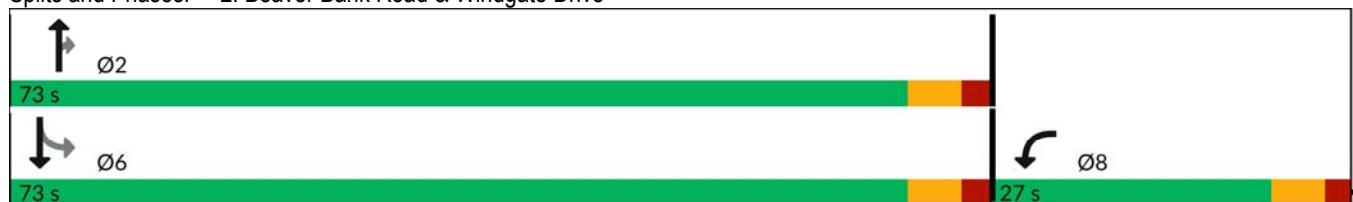
ICU Level of Service C

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 2: Beaver Bank Road & Windgate Drive



Intersection

Int Delay, s/veh 4.3

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|--------------------------|------|------|------|------|------|------|
| Lane Configurations | W | | T | ↑ | ↑ | |
| Traffic Vol, veh/h | 25 | 101 | 30 | 431 | 992 | 8 |
| Future Vol, veh/h | 25 | 101 | 30 | 431 | 992 | 8 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 25 | - | - | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 27 | 110 | 33 | 468 | 1078 | 9 |

| Major/Minor | Minor2 | Major1 | Major2 | | |
|----------------------|--------|--------|--------|---|---|
| Conflicting Flow All | 1616 | 1083 | 1087 | 0 | - |
| Stage 1 | 1083 | - | - | - | - |
| Stage 2 | 534 | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - |
| Pot Cap-1 Maneuver | 114 | 264 | 642 | - | - |
| Stage 1 | 325 | - | - | - | - |
| Stage 2 | 588 | - | - | - | - |
| Platoon blocked, % | | | | - | - |
| Mov Cap-1 Maneuver | 108 | 264 | 642 | - | - |
| Mov Cap-2 Maneuver | 108 | - | - | - | - |
| Stage 1 | 308 | - | - | - | - |
| Stage 2 | 588 | - | - | - | - |

| Approach | EB | NB | SB |
|------------------------|-------|------|----|
| HCM Control Delay, s/v | 51.85 | 0.71 | 0 |
| HCM LOS | F | | |

| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR |
|---------------------------|-------|-----|-------|-----|-----|
| Capacity (veh/h) | 642 | - | 205 | - | - |
| HCM Lane V/C Ratio | 0.051 | - | 0.667 | - | - |
| HCM Control Delay (s/veh) | 10.9 | - | 51.8 | - | - |
| HCM Lane LOS | B | - | F | - | - |
| HCM 95th %tile Q(veh) | 0.2 | - | 4.1 | - | - |

Lanes, Volumes, Timings

Total PM (2034)

1: Beaver Bank Road & Millwood Drive/Stokil Drive

10/11/2024

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|-----|-------|-------|-----|-------|--------|-----|-------|-------|-----|
| Lane Configurations | ↑ | ↑ | → | ↑ | ↑ | → | ↑ | ↑ | ↑ | ↑ | ↑ | ↑ |
| Traffic Volume (vph) | 118 | 49 | 122 | 93 | 76 | 95 | 143 | 967 | 90 | 22 | 503 | 98 |
| Future Volume (vph) | 118 | 49 | 122 | 93 | 76 | 95 | 143 | 967 | 90 | 22 | 503 | 98 |
| Satd. Flow (prot) | 1738 | 1629 | 0 | 1706 | 1684 | 0 | 1755 | 1831 | 0 | 1789 | 1794 | 0 |
| Flt Permitted | 0.287 | | | 0.322 | | | 0.249 | | | 0.058 | | |
| Satd. Flow (perm) | 524 | 1629 | 0 | 577 | 1684 | 0 | 460 | 1831 | 0 | 109 | 1794 | 0 |
| Satd. Flow (RTOR) | | 86 | | | 53 | | | 7 | | | 13 | |
| Lane Group Flow (vph) | 187 | 209 | 0 | 97 | 220 | 0 | 196 | 1140 | 0 | 32 | 664 | 0 |
| Turn Type | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 3 | 8 | | 7 | 4 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | 8 | | | 4 | | | 6 | | | 2 | | |
| Total Split (s) | 11.0 | 27.8 | | 11.0 | 27.8 | | 18.0 | 80.8 | | 11.0 | 73.8 | |
| Total Lost Time (s) | 4.0 | 6.2 | | 4.0 | 6.2 | | 4.0 | 6.4 | | 4.0 | 6.4 | |
| Act Effct Green (s) | 25.2 | 15.9 | | 25.2 | 15.9 | | 83.3 | 74.9 | | 76.6 | 67.2 | |
| Actuated g/C Ratio | 0.21 | 0.13 | | 0.21 | 0.13 | | 0.69 | 0.62 | | 0.63 | 0.56 | |
| v/c Ratio | 1.04 | 0.72 | | 0.52 | 0.82 | | 0.46 | 1.00 | | 0.19 | 0.66 | |
| Control Delay (s/veh) | 121.0 | 44.2 | | 48.7 | 63.0 | | 10.7 | 52.2 | | 10.0 | 23.6 | |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay (s/veh) | 121.0 | 44.2 | | 48.7 | 63.0 | | 10.7 | 52.2 | | 10.0 | 23.6 | |
| LOS | F | D | | D | E | | B | D | | A | C | |
| Approach Delay (s/veh) | 80.4 | | | 58.6 | | | 46.1 | | | 23.0 | | |
| Approach LOS | F | | | E | | | D | | | C | | |
| Queue Length 50th (m) | ~42.6 | 29.4 | | 19.5 | 41.0 | | 15.1 | ~308.8 | | 2.2 | 105.8 | |
| Queue Length 95th (m) | #41.9 | 50.8 | | 34.4 | 68.6 | | 20.7 | #410.8 | | 4.4 | 168.9 | |
| Internal Link Dist (m) | | 142.5 | | | 100.7 | | | 85.0 | | | 195.0 | |
| Turn Bay Length (m) | 90.0 | | | 50.0 | | | 90.0 | | | 60.0 | | |
| Base Capacity (vph) | 180 | 363 | | 186 | 346 | | 469 | 1138 | | 167 | 1034 | |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 | |
| Reduced v/c Ratio | 1.04 | 0.58 | | 0.52 | 0.64 | | 0.42 | 1.00 | | 0.19 | 0.64 | |

Intersection Summary

Cycle Length: 130.6

Actuated Cycle Length: 120.8

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 1.04

Intersection Signal Delay (s/veh): 46.6

Intersection LOS: D

Intersection Capacity Utilization 96.0%

ICU Level of Service F

Analysis Period (min) 15

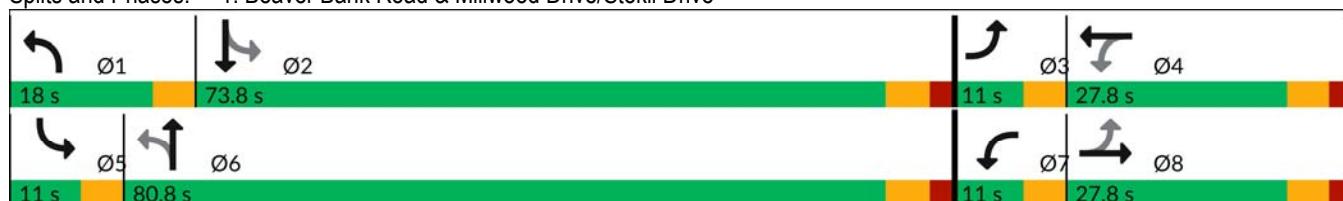
~ Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Beaver Bank Road & Millwood Drive/Stokil Drive



Lanes, Volumes, Timings
2: Beaver Bank Road & Windgate Drive

Total PM (2034)

10/11/2024



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|------------------------|-------|-----|-------|------|-------|------|
| Lane Configurations | ↑ ↗ | ↗ | ↑ | ↗ | ↖ | ↑ ↘ |
| Traffic Volume (vph) | 119 | 97 | 989 | 183 | 59 | 637 |
| Future Volume (vph) | 119 | 97 | 989 | 183 | 59 | 637 |
| Satd. Flow (prot) | 1721 | 0 | 1865 | 1601 | 1789 | 1865 |
| Flt Permitted | 0.973 | | | | 0.110 | |
| Satd. Flow (perm) | 1721 | 0 | 1865 | 1559 | 207 | 1865 |
| Satd. Flow (RTOR) | 34 | | | 91 | | |
| Lane Group Flow (vph) | 260 | 0 | 1063 | 213 | 77 | 777 |
| Turn Type | Prot | | NA | Perm | Perm | NA |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | | 2 | 6 | |
| Total Split (s) | 28.0 | | 82.0 | 82.0 | 82.0 | 82.0 |
| Total Lost Time (s) | 6.0 | | 6.0 | 6.0 | 6.0 | 6.0 |
| Act Effct Green (s) | 16.6 | | 57.5 | 57.5 | 57.5 | 57.5 |
| Actuated g/C Ratio | 0.19 | | 0.66 | 0.66 | 0.66 | 0.66 |
| v/c Ratio | 0.73 | | 0.86 | 0.20 | 0.56 | 0.63 |
| Control Delay (s/veh) | 44.4 | | 20.5 | 3.8 | 27.4 | 11.3 |
| Queue Delay | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay (s/veh) | 44.4 | | 20.5 | 3.8 | 27.4 | 11.3 |
| LOS | D | C | A | C | B | |
| Approach Delay (s/veh) | 44.4 | | 17.7 | | | 12.7 |
| Approach LOS | D | B | | | B | |
| Queue Length 50th (m) | 36.1 | | 122.9 | 6.6 | 6.1 | 66.2 |
| Queue Length 95th (m) | 67.1 | | 215.4 | 14.3 | 17.9 | 92.7 |
| Internal Link Dist (m) | 276.3 | | 119.4 | | | 97.2 |
| Turn Bay Length (m) | | | 25.0 | 40.0 | | |
| Base Capacity (vph) | 490 | | 1581 | 1336 | 175 | 1581 |
| Starvation Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.53 | | 0.67 | 0.16 | 0.44 | 0.49 |

Intersection Summary

Cycle Length: 110

Actuated Cycle Length: 87

Control Type: Semi Act-Uncoord

Maximum v/c Ratio: 0.86

Intersection Signal Delay (s/veh): 18.8

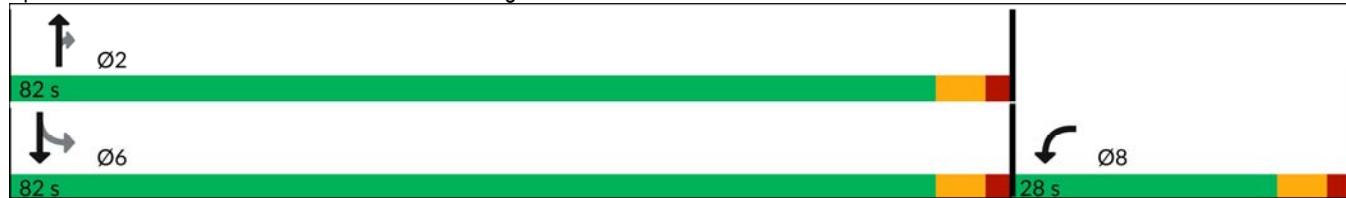
Intersection LOS: B

Intersection Capacity Utilization 74.6%

ICU Level of Service D

Analysis Period (min) 15

Splits and Phases: 2: Beaver Bank Road & Windgate Drive



| Intersection | | | | | | |
|-----------------------------|--------|--------|-------|--------|------|------|
| Int Delay, s/veh | 1.8 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | W | | T | ↑ | ↑ | |
| Traffic Vol, veh/h | 18 | 43 | 67 | 1019 | 653 | 28 |
| Future Vol, veh/h | 18 | 43 | 67 | 1019 | 653 | 28 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 25 | - | - | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 20 | 47 | 73 | 1108 | 710 | 30 |
| Major/Minor | Minor2 | Major1 | | Major2 | | |
| Conflicting Flow All | 1978 | 725 | 740 | 0 | - | 0 |
| Stage 1 | 725 | - | - | - | - | - |
| Stage 2 | 1253 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 68 | 425 | 866 | - | - | - |
| Stage 1 | 479 | - | - | - | - | - |
| Stage 2 | 269 | - | - | - | - | - |
| Platoon blocked, % | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 62 | 425 | 866 | - | - | - |
| Mov Cap-2 Maneuver | 62 | - | - | - | - | - |
| Stage 1 | 439 | - | - | - | - | - |
| Stage 2 | 269 | - | - | - | - | - |
| Approach | EB | NB | SB | | | |
| HCM Control Delay, s/v44.05 | | 0.59 | 0 | | | |
| HCM LOS | E | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR | |
| Capacity (veh/h) | 866 | - | 156 | - | - | |
| HCM Lane V/C Ratio | 0.084 | - | 0.424 | - | - | |
| HCM Control Delay (s/veh) | 9.5 | - | 44.1 | - | - | |
| HCM Lane LOS | A | - | E | - | - | |
| HCM 95th %tile Q(veh) | 0.3 | - | 1.9 | - | - | |